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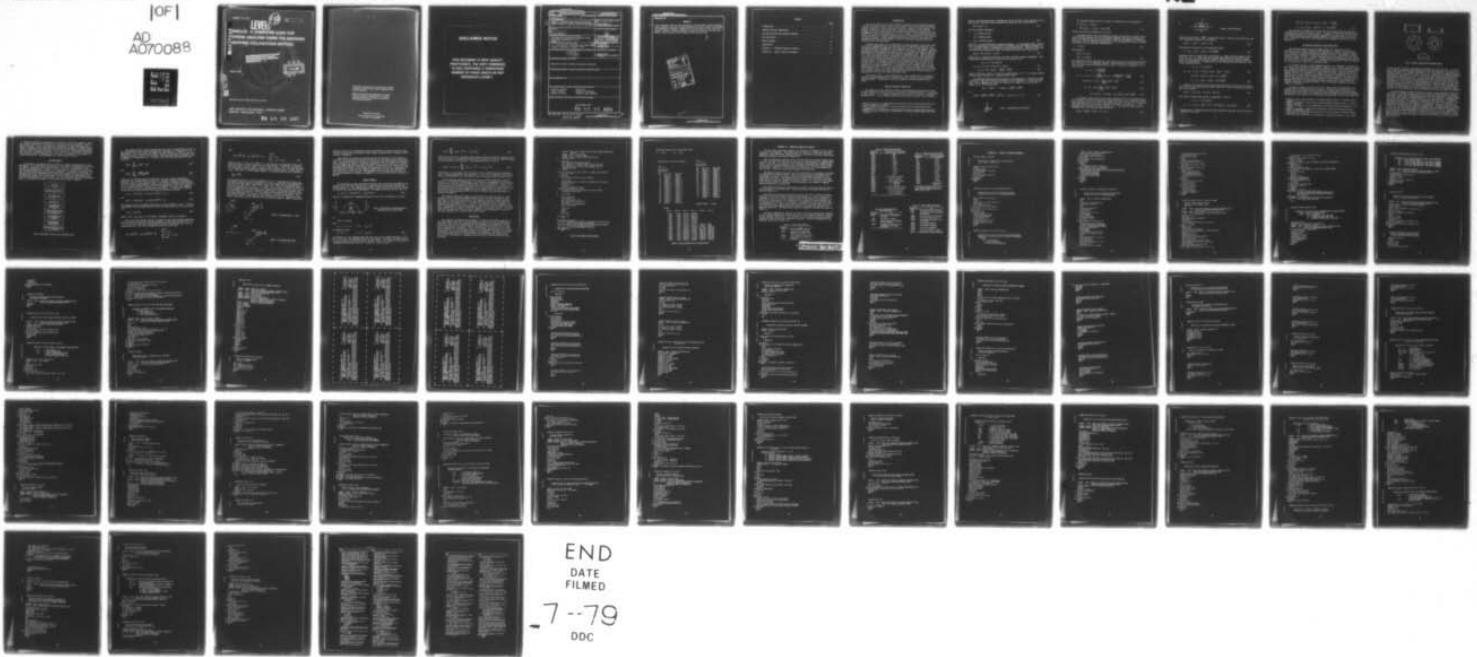
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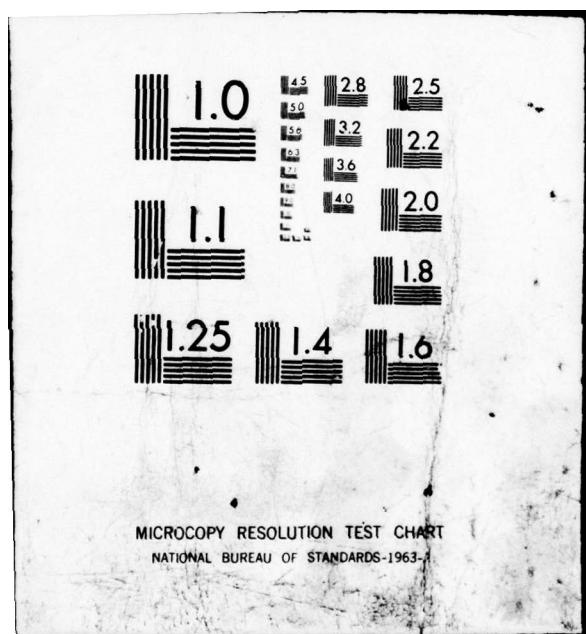
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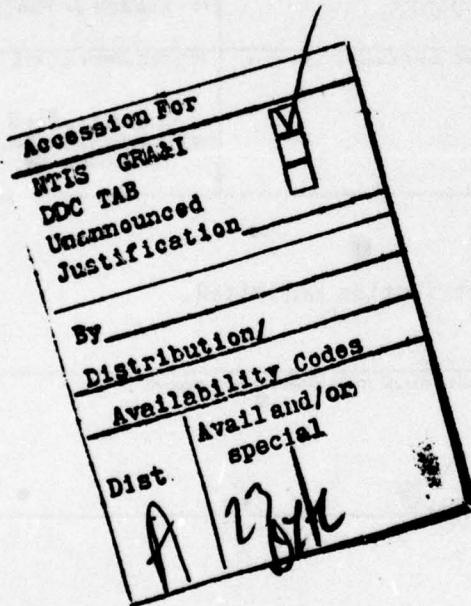
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**ABSTRACT**

→ A computer code for the solution of a wide variety of plane isotropic stress problems using the modified mapping-collocation method is presented. The mathematical approach, capabilities, and structure of the code are examined. Finally, a sample problem is solved to illustrate the ease with which stress solutions can be obtained utilizing the code.

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## INTRODUCTION

The stress analysis for plane problems in elasticity has been handled using a variety of methods, which include finite element and finite difference methods, integral equations, integral transform techniques, complex variable methods, and boundary collocation. One particularly versatile technique is the modified mapping-collocation (MMC) method<sup>1</sup> and the MMC method with partitioning<sup>2</sup> developed at AMMRC by a team of investigators led by O. L. Bowie. This method combines the complex variable and conformal mapping techniques of Muskhelishvili<sup>3</sup> with boundary collocation methods. Finite element representations have been introduced into problems analyzed by the MMC method by Freese,<sup>4</sup> resulting in greater potential versatility for the MMC method.

Previous exploitation of the MMC method to plane problems of practical interest has been hampered by the time-consuming task of algebraic manipulation and subsequent computer programming of the equations used in a given problem. Since the equations used are similar in each problem, the computer code MMCLIB (Modified Mapping-Collocation LIBrary) has been written to eliminate the algebraic manipulation effort and greatly minimize the computer programming task. MMCLIB consists of a library of ninety Fortran subroutines and functions which, when combined in a Fortran main program written by the user, have the ability to quickly provide stress solutions for plane problems while retaining the versatility inherent in the MMC method. Furthermore, addition of new mapping functions and series representations can be accomplished with a minimum of effort, which allows the expansion of the code's capabilities. The versatility of the MMC method has been demonstrated in the solution of a wide variety of stress problems such as sheets with internal flaws, i.e., cracks and ellipses, sheets with edge cracks and elliptical notches, sheets with cracks emanating from elliptical internal flaws and edge notches, and circular rings with edge cracks.

The current report is not intended to be a user's manual but is intended to describe the capabilities of the code MMCLIB in the solution of plane isotropic stress problems. Information on the use of MMCLIB can be obtained from the author.

## COMPLEX VARIABLE FORMULATION

The complex variable approach provides the mathematical formulation on which the MMC technique is based and results relating to the MMC method will be discussed in this section. For a complete treatment of the subject the reader is referred to Muskhelishvili.<sup>3</sup> A well-known method of describing the stresses in an isotropic

1. BOWIE, O. L., and NEAL, D. M. *A Modified Mapping Collocation Technique for Accurate Calculation of Stress Intensity Factors*. Int. J. Fracture Mech., v. 6, 1970, p. 199-206.
2. BOWIE, O. L., FREESE, C. E., and NEAL, D. M. *Solutions of Plane Problems of Elasticity Utilizing Partitioning Concepts*. J. Appl. Mech., v. 95, 1970, p. 767-772.
3. MUSKHELISHVILI, N. I. *Some Basic Problems of the Mathematical Theory of Elasticity*. Noordhoff, Groningen, Holland, 1953.
4. FREESE, C. E. *Collocation and Finite Elements - A Combined Method*. Army Materials and Mechanics Research Center, AMMRC TR 73-28, 1973.

elastic two-dimensional body is through the use of the Airy stress function,  $U(x, y)$ . Specifically, equilibrium and compatibility conditions will be satisfied if

$$\nabla^2 \nabla^2 U(x, y) = 0 \quad (1)$$

with the stresses defined by

$$\begin{aligned} \sigma_x &= [\partial^2 U(x, y)] / \partial y^2 \\ \sigma_y &= [\partial^2 U(x, y)] / \partial x^2 \\ \tau_{xy} &= [-\partial^2 U(x, y)] / \partial x \partial y \end{aligned} \quad (2)$$

where  $\nabla^2$  is the two-dimensional Laplacian operator. In the Muskhelishvili formulation, the coordinates of the problem are described using the complex variable  $z = x + iy$  and the  $z$ -plane is referred to as the physical plane. The Airy stress function can then be represented using two analytic functions  $\phi_z(z)$  and  $\psi_z(z)$  by

$$U(x, y) = \operatorname{Re} [\bar{z} \phi_z(z) + X_z(z)] \quad (3)$$

where  $\psi_z(z) = d X_z / dz$ ,  $\operatorname{Re}$  means the real part, and bars complex conjugation. The stresses and displacements in terms of  $\phi_z(z)$  and  $\psi_z(z)$  are

$$\begin{aligned} \sigma_x + \sigma_y &= 4 \operatorname{Re} [\phi_z'(z)] \\ \sigma_y - \sigma_x + 2i \tau_{xy} &= 2[\bar{z} \phi_z''(z) + \psi_z'(z)] \end{aligned} \quad (4)$$

$$2G(u + iv) = k\phi_z(z) - z\bar{\phi}_z(z) - \bar{\psi}_z(z) \quad (5)$$

with  $G = E/2(1+v)$ , and  $k = (3-v)/(1+v)$  (plane stress), or  $k = 3-4v$  (plane strain),  $E$  being Young's modulus and  $v$  being Poisson's ratio.

An additional physical quantity which is used frequently in applying the MMC technique is the force acting on an arbitrary arc of material. If  $X_{nds}$  and  $Y_{nds}$  are  $x$ - and  $y$ -components of the force acting on an element of the arc  $ds$  (see Figure 1), it can be shown that

$$(X_n + i Y_n)ds = -i d \{ \phi_z(z) + z\bar{\phi}_z(z) + \bar{\psi}_z(z) \}$$

or

$$\phi_z(z) + z\bar{\phi}_z(z) + \bar{\psi}_z(z) = i \int (X_n + i Y_n) ds = f_1 + i f_2. \quad (6)$$

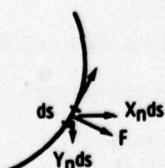


Figure 1. Forces acting on an arc of material.

The resultant moment about the origin of coordinates can be expressed as

$$M = \int (x Y_n - y X_n) ds \\ = \operatorname{Re} [X_z(z) - z \psi_z(z) - z \bar{z} \phi'(z)]_A^B \quad (7)$$

where A and B are the endpoints of the arc.

The formulation of the two-dimensional theory of elasticity in terms of analytic functions permits the use of conformal mapping techniques, providing the means to introduce curvilinear coordinates to describe the geometry in the physical plane. Use of conformal mappings leads to the introduction of the  $\zeta$  or parameter plane with the conformal transformation

$$z = \omega(\zeta). \quad (8)$$

The functions

$$\phi(\zeta) = \phi_z(\omega(\zeta)) \\ \psi(\zeta) = \psi_z(\omega(\zeta)) \quad (9)$$

are therefore analytic functions of  $\zeta$  since  $\phi_z(z)$  and  $\psi_z(z)$  are analytic functions of  $z$  and  $\omega(\zeta) = z$  is a conformal mapping. Substituting  $\phi(\zeta)$  and  $\psi(\zeta)$  for  $\phi_z(z)$  and  $\psi_z(z)$  and using relationships such as  $\phi'_z(z) = \phi'(\zeta)/\omega'(\zeta)$ , Equations 4, 5, 6, and 7 become

$$\sigma_x + \sigma_y = 4 \operatorname{Re} \left[ \frac{\phi'(\zeta)}{\omega'(\zeta)} \right] \\ \sigma_y - \sigma_x + 2i \tau_{xy} = 2 \frac{\omega(\zeta)}{(\omega'(\zeta))^2} (\phi''(\zeta) - \frac{\omega''(\zeta)\phi'(\zeta)}{\omega'(\zeta)}) + \frac{\psi'(\zeta)}{\omega'(\zeta)} \quad (10)$$

$$2G(u+iv) = k \phi(\zeta) - \frac{\omega(\zeta)}{\omega'(\zeta)} \overline{\phi'(\zeta)} - \overline{\psi(\zeta)} \quad (11)$$

$$f_1 + if_2 = \phi(\zeta) + \frac{\omega(\zeta)}{\omega'(\zeta)} \overline{\phi'(\zeta)} + \overline{\psi(\zeta)} \quad (12)$$

$$M = \operatorname{Re} [X(\zeta) - \omega(\zeta)\psi(\zeta) - \omega(\zeta) \overline{\omega(\zeta)} \phi'(\zeta)/\omega'(\zeta)]_A^B. \quad (13)$$

An extremely useful result of the work of Muskhelishvili is the application of the analytic continuation arguments summarized below. Let  $S^+$  denote the region above the real axis ( $y > 0$ ) and  $S^-$  the region below the real axis ( $y < 0$ ) and further assume that the elastic body occupies the region  $S^+$  (see Figure 2). The functions  $\phi_z(z)$  and  $\psi_z(z)$  are thus defined in  $S^+$ . The functions  $\phi_z(z)$  shall be continued into  $S^-$  by the following definition:

$$\phi_z(z) = -z \overline{\phi}'(z) - \overline{\psi}_z(z) \quad \text{for } z \in S^-, \quad (14)$$

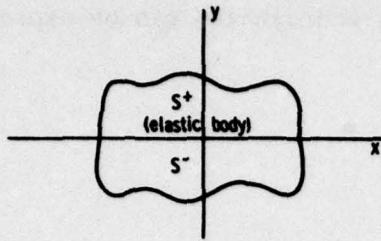


Figure 2. Analytic continuation.

with the notation  $\bar{f}(z) = \overline{f(\bar{z})}$ . Noting that if  $z \in S^-$ , then  $z \in S^+$  and taking the complex conjugate of Equation 14 one finds

$$\psi_z(z) = -\bar{\phi}_z(z) - z \phi_z'(z), \quad z \in S^+. \quad (15)$$

Substitution of Equation 15 into Equation 6 gives

$$f_1 + if_2 = \phi_z(z) - \phi_z(\bar{z}) + (z - \bar{z}) \overline{\phi_z'(z)}. \quad (16)$$

Evaluation of this equation for  $z$  with  $\text{Im}(z) = 0$ , where  $\text{Im}$  means imaginary part, gives  $f_1 + if_2 = 0$ . Thus, the real axis has been defined as load-free, while  $\psi_z(z)$  has been eliminated from the analysis leaving only the analytic function  $\phi_z(z)$  to be determined. If Equation 15 is also substituted into Equations 4 and 5 the following results:

$$\sigma_x + \sigma_y = 4 \text{ Re } [\phi_z'(z)]$$

$$\sigma_y - \sigma_x + 2i \tau_{xy} = 2 [(\bar{z} - z) \phi_z''(z) - \bar{\phi}_z'(z) - \phi_z'(z)] \quad (17)$$

$$2 G(u+iv) = k\phi_z(z) + \phi_z(\bar{z}) + (\bar{z} - z) \overline{\phi_z'(z)}$$

$$f_1 + if_2 = \phi_z(z) - \phi_z(\bar{z}) + (z - \bar{z}) \overline{\phi_z'(z)} \quad (18)$$

Similarly the function  $\phi_z(z)$  can be continued from the exterior of the unit circle ( $S^+$ ) to the interior of the unit circle ( $S^-$ ) using the following definition due to Kartzivadze<sup>5</sup>

$$\phi_z(z) = -z \bar{\phi}_z'(1/z) - \bar{\psi}_z(1/z) \quad \text{for } z \in S^-. \quad (19)$$

This leads to expressions similar to Equations 17 and 18

$$\sigma_x + \sigma_y = 4 \text{ Re } [\phi_z'(z)]$$

$$\sigma_y - \sigma_x + 2i \tau_{xy} = 2[(\bar{z} - 1/z) + 1/z^2 \bar{\phi}_z'(1/z) + 1/z^2 \phi_z'(z)] \quad (20)$$

5. KARTZIVADZE, I. N. *The Fundamental Problems of the Theory of Elasticity for the Elastic Circle*. Comp. Rend. de L'acad. Sc. de l'URSS, v. 20, 1943, p. 95-104.

$$2 G(u+iv) = k\phi_z(z) + \phi_z(1/z) + (1/\bar{z} - z) \overline{\phi'_z(z)}$$

$$f_1 + if_2 = \phi_z(z) - \phi_z(1/\bar{z}) + (z - 1/\bar{z}) \overline{\phi'_z(z)}. \quad (21)$$

The evaluation of Equation 21 on the unit circle shows that traction-free conditions must exist on the unit circle. It should be noted that the definitions in Equations 19 and 13 for the analytic continuation of  $\phi_z(z)$  from  $S^+$  to  $S^-$  will need slight modification when conformal mapping is included in the analysis and  $\phi(\zeta) = \phi_z(\omega(\zeta))$  is used due to the presence of the mapping function in the force Equation 12.

### THE MODIFIED MAPPING-COLLOCATION METHOD

The modified mapping-collocation (MMC) method is a technique for two-dimensional elastic stress analysis which combines the complex variable formulation and conformal mapping arguments of Muskhelishvili<sup>3</sup> and the boundary collocation technique, retaining the attractive features of each. This method was first proposed by Bowie and Neal,<sup>1</sup> and was refined with the introduction of a partitioning plan by Bowie, Freese, and Neal.<sup>2</sup> The MMC method has subsequently been applied to a wide variety of problems,<sup>6-11</sup> illustrating its versatility. Refer to Figure 3 for illustrations of some of the problems solved.

In the MMC technique a simple mapping function as in Equation 7 is chosen to describe critical portions of the physical geometry, e.g., cracks, notches, cutouts, etc. Remaining portions of the geometry can be described by inversion of the plane mapping function from the physical to the parameter plane. Thus, the forms of the mapping functions are algebraically simple since the entire geometry need not be described by a single function, and greater versatility is obtained since a unique mapping function need not be obtained for each problem geometry. The specification in the parameter plane of those portions of the boundary not described by the mapping function may be algebraically complex, making direct specification of boundary conditions extremely difficult. For this reason a boundary collocation scheme is introduced.

In order to obtain  $\phi(\zeta)$  and  $\psi(\zeta)$  for the problem under consideration a representation for each function must be chosen. Generally, when analyticity is assured, power and Laurent series are chosen for representation, and the unknown coefficients of the series are determined using the boundary collocation arguments. The forms for  $\phi(\zeta)$  and  $\psi(\zeta)$  are substituted into Equations 10 to 13, and equations

6. BOWIE, O. L. *Methods of Analysis and Solutions of Crack Problems in Mechanics of Fracture*, v. 1, G. C. Sih, ed., Noordhoff, Leden, 1973.
7. BOWIE, O. L., and FREESE, C. E. *Analysis of Notches Using Conformal Mapping* in Mechanics of Fracture, v. 5, G. C. Sih, ed., Noordhoff, Leden, 1978.
8. BOWIE, O. L., and FREESE, C. E. *On the 'Overlapping' Problem in Crack Analysis*. Engineering Fracture Mechanics, v. 8, 1976, p. 373-379.
9. BOWIE, O. L., and FREESE, C. E. *Elastic Analysis for a Radial Crack in a Circular Ring*. Army Materials and Mechanics Research Center, AMMRC MS 70-3, 1970.
10. TRACY, P. G. *Elastic Analysis of Radial Cracks Emanating from the Outer and Inner Surfaces of a Circular Ring*. Engineering Fracture Mechanics, v. 11, 1979, p. 291.
11. TRACY, P. G. *Analysis of a Radial Crack in a Circular Ring Segment*. Engineering Fracture Mechanics, v. 7, 1975, p. 253-260.

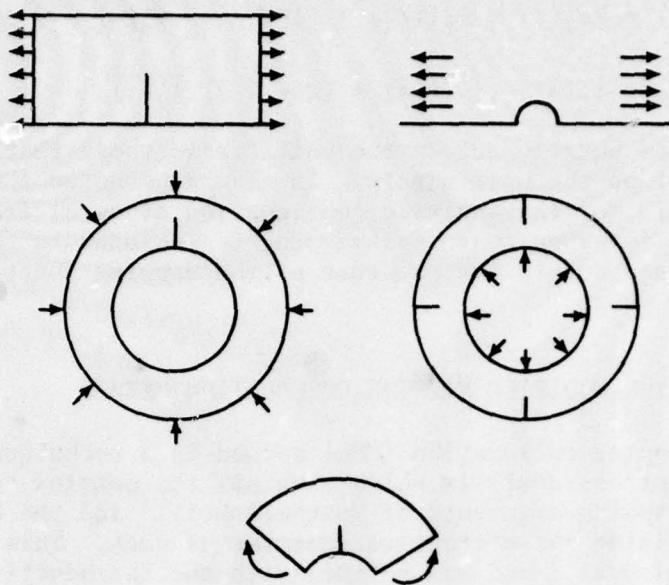


Figure 3. Examples of problems solved using MMC method.

can be written in terms of the unknown coefficients of  $\phi(\zeta)$  and  $\psi(\zeta)$ . In situations where the representations for  $\phi(\zeta)$  and  $\psi(\zeta)$  are complete, collocation of  $f_1$  and  $f_2$  (Equation 12) is usually sufficient. In a region with a crack tip near a boundary, error in matching  $f_1$  and  $f_2$  may result, indicating the need for collocating stresses, Equation 10, as well as  $f_1$  and  $f_2$ , particularly on the portion of the boundary near the crack tip. In cases where the representation may not be complete, the collocation of  $M$ , Equation 13, as well as forces and stresses may be required. A set of points on the boundaries is chosen at which to write equations such that the number of equations generated is greater than the number of unknown coefficients by at least a factor of two. A least-squares minimization of error is used to generate a linear system of equations in the unknown coefficients; the coefficients can then be determined by solving the system of equations.

The partitioning concepts introduced by Bowie, Freese, and Neal<sup>2</sup> extend the flexibility of the MMC technique to allow solutions for problems which are awkward with a single series representation for the stress functions. Such problems occur when, for example, singularities occur near the circles of convergence for the stress functions due to areas of high stress concentrations. To implement the partitioning plan, the geometry is subdivided into two or more regions. The functions  $\phi_z(z)$  and  $\psi_z(z)$  are defined in a subregion  $i$  by  $\phi_{z,i}(z)$  and  $\psi_{z,i}(z)$ , along with a mapping for each region, if appropriate. Boundary conditions (Equations 10 to 13) are enforced along the boundary using the appropriate  $\phi_{z,i}(z)$  and  $\psi_{z,i}(z)$  for the collocation point at which equations are written. Additionally, at points on the common boundaries of zones  $u+iv$  and  $f_1 + if_2$  are equated to assure continuity of  $\phi_z(z)$  and  $\psi_z(z)$ . Then the least-squares procedure is invoked and the resulting equations solved to obtain the function  $\phi_{z,i}(z)$  and  $\psi_{z,i}(z)$  in each subregion.

Once the solution is obtained it is necessary to assess the degree to which the boundary conditions are satisfied by  $\phi_z(z)$  and  $\psi_z(z)$  as obtained. This is done in two ways. First, the solution is recomputed, varying the number and location of points at which equations are written and the number of unknown coefficients to confirm that a wide range of these choices will yield the same results, thus assuring a convergent solution. As a second check, the boundary conditions are evaluated using the computed  $\phi_z(z)$  and  $\psi_z(z)$  and compared to the values required for solution. Good agreement will assure correct results.

### THE CODE MMCLIB

The computer code MMCLIB has been written to enhance implementation of the MMC method. To retain maximum flexibility in the variety of problems to be solved, the code is constructed in a modular fashion. The user is required to write a Fortran main program which usually is 30 to 100 lines in length and uses the modules (Fortran subroutines and functions) of MMCLIB. In addition, the modular construction allows the implementation of additional mapping functions and series representation types as one need program only the function or representation and its first two derivatives into the code. Let us now consider the solution process, which is illustrated in Figure 4, and examine the features of MMCLIB.

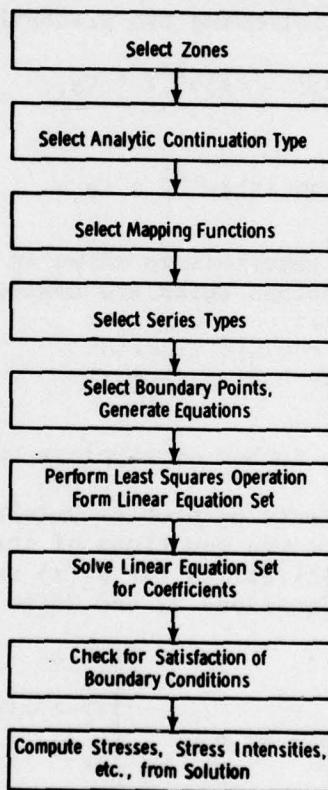


Figure 4. Block diagram of solution process using MMC method.

The problem geometry under consideration must first be subdivided into one or more subregions or zones with reflections as in Equation 14 or Equation 19, if appropriate. This will define the number and type (either  $\phi_{z,i}(z)$  or  $\psi_{z,i}(z)$ ) of functions needed to complete the solution. Each such function is defined by zone in MMCLIB by a subroutine call. At present two functional representations are available:

$$f_1(W) = \sum_{n=-N}^M a_n (W^n - W_0)^n \quad (22)$$

and

$$f_2(W) = \sum_{n=-N}^M \frac{a_n (W^n - W_0)^n}{W+i} \quad (23)$$

where  $a_n$  is an unknown complex coefficient,  $W$  is the (complex) parametric-coordinate or  $z$ -coordinate in the case of no mapping,  $M$  and  $N$  are nonnegative integers, and  $W_0$  is the expansion point. A function is defined by specifying  $W_0$ ,  $M$ ,  $N$ , the series representation, the material parameters of that zone, and any real or imaginary parts of  $a_n$  for even or odd powers of  $n$  which are assumed to be zero due to the stress symmetries of the problem. For each zone a mapping function may be chosen from the following two presently available

$$\omega_1(\zeta) = [(a_1+b_1)\zeta/2 + (a_1-b_1)\zeta^{-1}/2]e^{i\theta_1} + \zeta_{0,1} \quad (24)$$

and

$$\omega_2(\zeta) = i[b_2 \cosh(i\zeta) - a_2 \sinh(i\zeta)]e^{i\theta_2} + \zeta_{0,2}. \quad (25)$$

The action of these two mapping functions is shown in Figures 5 and 6. In addition, MMCLIB allows mapping functions which are compositions of  $\omega_1(\zeta)$  and  $\omega_2(\zeta)$ , i.e.,

$$\omega(\zeta) = \omega_i[\omega_j(\zeta)] \quad (26)$$

where  $i$  and  $j$  vary from 1 to the number of mappings currently available.

One of the most tedious aspects of problem solving using the MMC method has been the need to algebraically reduce equations of the type Equations 10 to 13, 17, 18, 20, and 21 with the substitutions for  $\phi_z(z)$  and  $\psi_z(z)$  or  $\phi(\zeta)$ ,  $\psi(\zeta)$  of representations of the form of Equations 22 and 23 to the form

$$[a_{nr} f_{rr}^{(n)}(W) + a_{ni} f_{ri}^{(n)}(W)] = \operatorname{Re} \begin{cases} u+iv \\ f_1 + if_2 \\ \sigma_y - \sigma_x + 2i \tau_{xy} \\ 4 \phi_z'(z) \end{cases}$$

and

$$[a_{nr} f_{ir}^{(n)}(W) + a_{ni} f_{ii}^{(n)}(W)] = \text{Im} \begin{cases} u+iv \\ f_1 + if_2 \\ \sigma_y - \sigma_x + 2i \tau_{xy} \end{cases} \quad (27)$$

where  $a_n = a_{nr} + i a_{ni}$ ,  $W$  is either  $\zeta$  or  $z$  and the  $f$ 's are functions of the position of the point at which equations are being written. Collocation of forms for functions such as  $\alpha\phi_z(z)$ ,  $\alpha\phi_z'(z)$ ,  $\alpha\phi_z''(z)$ ,  $\alpha\phi_z(\bar{z})$ ,  $\alpha\phi_z(z)$ , etc., are each contained in a subroutine, and equations are generated by successive calls to these subroutines. Note that  $\alpha$  is some complex number. The form assumed for each function is

$$\sum_n a_n f_n(W) \quad (28)$$

where presently  $f_n(W)$  is either of Equation 22 or 23. Other forms for  $f_n(W)$  can be added by simply inserting programming for  $f_n(W)$ ,  $[df_n(W)/dW]$ , and  $[d^2f_n(W)/d^2W]$  into the three appropriate subroutines. Many of the forms for the mapping functions such as  $\omega(\zeta)$ ,  $\omega(\bar{\zeta})$ ,  $\omega'(\zeta)$ ,  $\omega''(\zeta)$ ,  $\bar{\omega}(\zeta)$ , etc., are also contained in modules for use in generation of equations. It should be noted that if  $\omega_1(\zeta)$ ,  $\omega_1'(\zeta)$ ,  $\omega_1''(\zeta)$  are programmed into the three appropriate subroutines, the mapping function  $\omega_1(\zeta)$  can be included for analysis. Certain commonly used equations for problem solving have been programmed into modules using previously described subroutines. Thus, equations for forces, displacements, and stresses for real axis reflections, unit circle reflections, and no reflection are contained in modules. MMCLIB, therefore,

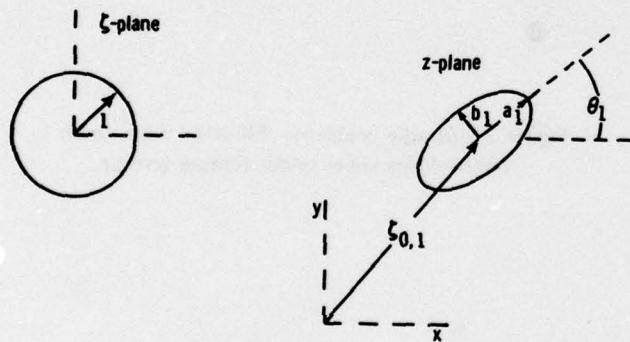


Figure 5. The mapping function  $z = \omega_1(\zeta)$ .

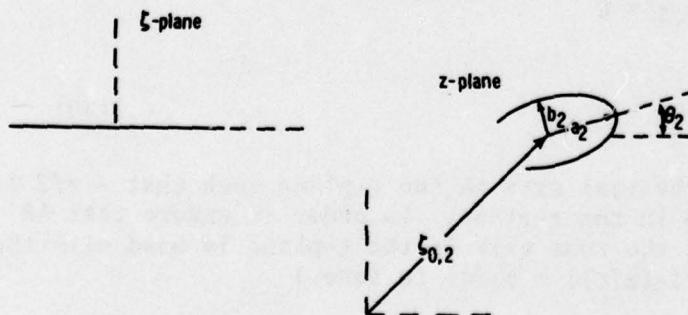


Figure 6. The mapping function  $\omega_2(\zeta)$ .

eliminates most of the repetitious equation derivation, allowing the user to concentrate on modelling the problem at hand without spending time in algebraic manipulation of equations.

After points are chosen for collocation and the equations in the unknown coefficients are generated and solved, the results of the computations can be examined. Any physical quantity can then be calculated using the computed coefficients and the appropriate modules to generate equations for the quantities of interest. The more common physical quantities of stress, displacements, and forces have been programmed into modules to facilitate the acquisition of results. Subroutines are also available to print out the computed coefficients and the input information about the various series in use. See Appendix A for the names and functions of the important modules of MMCLIB and Appendix B for the Fortran source listings for MMCLIB.

### SAMPLE PROBLEM

To illustrate the ease with which solutions can be obtained using MMCLIB, the problem of an elliptical edge notch in a semi-infinite sheet under tension was solved (Figure 7). This problem was studied by Bowie and Freese<sup>7</sup> and their method of solution was duplicated using MMCLIB. The mapping function used for zone I is

$$z = \omega(\zeta) = i [(a+b)e^{-i\zeta/2} - (a-b)e^{i\zeta/2}] \quad (29)$$

which is a composition of mapping functions of the type in Equations 24 and 25.

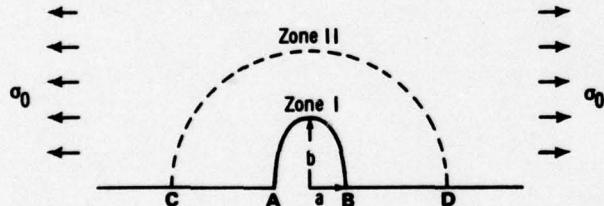


Figure 7. Sample problem: Elliptical edge notch in semi-infinite sheet under remote tension.

If

$$\omega(\zeta) = \omega_1(\omega_2(\zeta))$$

then

$$a_1 = a \quad b_1 = b \quad \theta_1 = 0 \quad \zeta_{0,1} = 0$$

in Equation 24 and

$$a_2 = b_2 = 1 \quad \theta = 0 \quad \zeta_{0,2} = 0 \quad (30)$$

in Equation 25. This mapping takes the real axis in the  $\zeta$ -plane such that  $-\pi/2 \leq \operatorname{Re} \zeta \leq \pi/2$  into the elliptical arc AB in the z-plane. In order to ensure that AB is traction-free, a reflection across the real axis in the  $\zeta$ -plane is used with the following representation for  $\phi_z(z) = \phi_z(\omega(\zeta)) = \phi_I(\zeta)$  in zone I

$$\phi_I(\zeta) = \sum_{n=1}^{N_1} [a_{2n-1} \zeta^{2n-1} + i a_{2n} \zeta^{2n}] \quad (31)$$

where the a's are real, ensuring stress symmetry about the physical imaginary axis. In zone II there is no mapping function and a reflection is used to ensure traction-free conditions on the real axis. The representation for  $\phi_2(z)$  is

$$\phi_{II}(z) = (1/4) \sigma_0 + \sum_{n=0}^{N_2} [a_{-2n-1} z^{-2n-1} + i a_{-2n} z^{-2n}] \quad (32)$$

ensuring  $\sigma_x = \sigma_0$  for large  $z$  and the proper stress symmetry about the imaginary axis. Along the segment BD the condition  $f_1 + i f_2 = 0$  is collocated, and the condition of continuity of  $f_1 + i f_2$  and  $u + iv$  are collocated on the circular arc CD.

The Fortran main program used in the solution of this problem is shown in Figure 8 to illustrate the magnitude of the computer programming effort necessary to carry out a solution using the MMC method with the code MMCLIB. Lines 8 to 12 define the series and mapping functions to be used and lines 16 to 20 and 22 to 30 find points and collocate equations on the curves BD and DE, respectively. The printing of results of the computations are programmed into lines 34 to 40. It can be seen that programming effort to solve a problem using the MMC method is minimal with MMCLIB.

The computer generated output for this problem is shown in Figure 9. The maximum stress as computed by MMCLIB compares well with that computed by Bowie and Freese. The error calculation in this example is typical of many problems. Note that the right-hand sides of the equations generated are of the order of magnitude of the coordinates (i.e., unity). The amount of error compared to the order of magnitude of the values desired as shown in the first two columns of the error computation are usually considered adequate for accurate results. The third and fourth columns and fifth and sixth columns are the coordinates in zones one and two, respectively, at which errors were checked.

### CONCLUSIONS

The computer code MMCLIB should permit a savings in the effort involved in obtaining stress solutions to plane problems of elasticity using the MMC method since the effort will be concentrated on the mathematical and physical concepts involved in solving the problems and not on mechanical activities such as algebraic manipulation of equations. Thus, problems whose solutions are not conceptually difficult to the experienced user of the MMC method but which were tedious to implement can be solved almost routinely using MMCLIB. Furthermore, research into further development of the MMC method can be performed much more easily since most of the analyst's attention can be focused on the new features being developed.

```

DIMENSION X(50),Y(50),XP(50),YP(50),F1(50),F2(50),U(50),V(50),
*          GPAR(5)
COMMON /MAT/ G(5),ETAM(5)
COMMON /PIFAC/ PI,HLFPI,TWOP1
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
DATA GPAR /5*0./
C
CALL INIT
READ 1000,IPOS,INEG,NPT,NST,AA,BB
CALL SERINF(1,1,1,0,IPOS,0,1001,1,0.,0.,1.E+7,.3)
CALL SERINF(2,1,1,INEG,0,1,1001,1,0.,0.,1.E+7,.3)
CALL MAPINF(1,2,1.,1.,0.,0.,0.,1,AA,BB,0.,0.,0.)
RZ=AMAX1(AA,BB)*2.
IERR=0
C
100 CALL POINTF(1,AA,0.,RZ,0.,NPT,1,1,1,GPAR,1,2,X,Y,XP,YP)
DO 110 I=1,NPT
F1(I)=0.
110 F2(I)=0.
CALL FDCOL(XP,YP,NPT,1,1,2,F1,F2,IERR)
C
GPAR(1)=RZ
CALL POINTF(1,RZ,0.,0.,RZ,NST,0,0,2,GPAR,0,2,X,Y,XP,YP)
DO 120 I=1,NST
F1(I)=0.
F2(I)=Y(I)
U(I)=X(I)*(ETAM(1)+1.)*.25
120 V(I)=Y(I)*(ETAM(1)-3.)*.25
CALL STITCH(1,2,2,2,3,2,0,NST,X,Y,F1,F2,U,V,IERR)
IF(IERR.EQ.1)GO TO 130
C
CALL FNDMAT
C
PRINT 1002,AA,BB
CALL PRTCDF(12)
CALL ZERO(1,2,1,2,3,0)
CALL PHIP(.0001,0.,4./AA,0.,1)
CALL PLACE(1,1,1,1,1,1)
CALL EVAL(1,1,1,STRMAX,SDUM)
PRINT 1003,STRMAX
C
PRINT 1001
IERR=1
NST=6
NPT=10
GO TO 100
C
130 PRINT 1004
STOP
C
1000 FORMAT(4I5,2E10.4)
1001 FORMAT(7H0ERRORS//4X,7HERROR 1,3X,7HERROR 2,3X,6HCOR 1R,4X,
*          6HCOR 1I,4X,6HCOR 2R,4X,6HCOR 2I)
1002 FORMAT(45H1ELLIPTICAL EDGE NOTCH IN SEMI-INFINITE SHEET//)
*          4H A =,F8.4,10X,3HB =,F8.4////)
1003 FORMAT(///17H MAXIMUM STRESS =,F8.4////)
1004 FORMAT(1H1)
END

```

Figure 8. Main program for sample problem.

ELLIPTICAL EDGE NOTCH IN SEMI-INFINITE SHEET

A = .1250

B = .5000

COEFFICIENTS IN PHI, PSI FUNCTIONS

ZONE NO. 1

PHI FUNCTION  
SERIES TYPE 1

POW	REAL COEF	IMAG COEF
0	.00000	.00000
1	.30070+00	.00000
2	.00000	.39187-01
3	-.40076-01	.00000
4	.00000	-.85981-02
5	.38902-02	.00000
6	.00000	-.16099-03
7	.22604-03	.00000
8	.00000	-.17401-04
9	.51200-04	.00000
10	.00000	.11194-04
11	.41939-05	.00000
12	.00000	.13837-05
13	.13354-05	.00000
14	.00000	.13379-05
15	-.37054-06	.00000
16	.00000	-.36768-07
17	.35488-07	.00000
18	.00000	.55372-07
19	-.23934-07	.00000
20	.00000	-.44828-08

ZONE NO. 2

PHI FUNCTION  
SERIES TYPE 1

POW	REAL COEF	IMAG COEF
-20	.00000	.34927-05
-19	-.19418-04	.00000
-18	.00000	-.47040-04
-17	.63436-04	.00000
-16	.00000	.32696-04
-15	.17873-04	.00000
-14	.00000	.47948-04
-13	-.11984-04	.00000
-12	.00000	.77529-04
-11	-.14141-03	.00000
-10	.00000	-.14408-03
-9	.19836-03	.00000
-8	.00000	.28798-03
-7	-.67002-03	.00000
-6	.00000	-.12855-02
-5	.34014-02	.00000
-4	.00000	.63706-02
-3	-.19156-01	.00000
-2	.00000	-.33425-01
-1	.16262+00	.00000
0	.00000	.22439+00

MAXIMUM STRESS = 9.6224

ERRORS

ERROR 1	ERROR 2	COR 1R	COR 1I	COR 2R	COR 2I
-.0003	-.0006	.1571+01	.1888+00		
-.0003	-.0000	.1571+01	.3640+00		
.0005	-.0000	.1571+01	.5239+00		
.0001	.0000	.1571+01	.6688+00		
-.0003	.0003	.1571+01	.7998+00		
-.0001	.0001	.1571+01	.9187+00		
.0001	-.0003	.1571+01	.1027+01		
.0000	-.0001	.1571+01	.1126+01		
.0001	.0004	.1571+01	.1217+01	.1000+01	.0000
.0000	-.0000	.1571+01	.1217+01	.1000+01	.0000
.0000	.0001	.1287+01	.1209+01	.9511+00	.3090+00
-.0000	-.0001	.1287+01	.1209+01	.9511+00	.3090+00
-.0001	-.0001	.9949+00	.1185+01	.8090+00	.5878+00
.0000	.0000	.9949+00	.1185+01	.8090+00	.5878+00
.0001	.0001	.6866+00	.1150+01	.5878+00	.8090+00
-.0000	-.0001	.6866+00	.1150+01	.5878+00	.8090+00
-.0000	-.0001	.3542+00	.1114+01	.3090+00	.9511+00
.0000	.0001	.3542+00	.1114+01	.3090+00	.9511+00
-.0000	.0001	.2980-07	.1099+01	.1589-07	.1000+01
.0000	-.0000	.2980-07	.1099+01	.1589-07	.1000+01

Figure 9. Computer generated output for sample problem.

## APPENDIX A. IMPORTANT MODULES OF MMCLIB

In this section the more commonly used subroutines of MMCLIB will be listed and their uses explained. The subroutines are broken up by function into five groupings: Zone Definition, Mapping Functions, Function Collocation, Specialized Equation Generation, and Results Computation.

The Zone Definition routines allow the definition of functions (either  $\phi_z(z)$  or  $\psi_z(z)$ ) in each zone to be used in the analysis and definition of mapping functions in each zone. In addition, the functional representations, material properties, and any unknowns needed but not included in the functional forms chosen are defined. Note that all zone definition subroutine calls are preceded by a call to INIT. Table A-1 lists these routines and their uses.

The Mapping Function routines allow the calculation of coordinates in either the parametric or physical plane. These routines are used in determination of coordinates of points in one plane when the corresponding coordinates in the other plane are known. The Mapping Function routines and the forms of the mapping function which they compute are listed in Table A-2. Note that some subroutines return a number of functional forms depending on the number of mapping functions defined in a given zone.

The Function Collocation subroutines are used to write equations for the unknown parameters of the functions. Several Function Collocation routines are listed in Table A-3.

The Specialized Equation Generation routines are used to generate multiple equations for the most commonly used physical quantities. These routines are frequently used since in most solutions using the MMC method, the equations collocated on a given part of the boundary of the configuration being studied are of the same type and thus it is convenient to generate all these equations with one subroutine call. Specialized Equation Generation routines make use of Function Collocation and Mapping Function routines to generate the equations for physical quantities. The Specialized Equation Generation routines are listed in Table A-4.

The Result Computation routines are used to print the coefficients computed in the solution and physical quantities which can be obtained using the solution for the unknown coefficients. The routines are also used to print the various parameters input in the zone information routines. The Result Computation subroutines are listed in Table A-5.

Table A-1. ZONE DEFINITION ROUTINES

Subroutine	Use
INIT	Initialize MMCLIB variables
SERINF	Define functions and material properties to be used in zone
MAPINF	Define mapping function in zone
CONINF	Define unknown not contained in functions

Table A-2. MAPPING FUNCTION ROUTINES

Subroutine	Mapping Function Calculated
MAP8	$\omega(\zeta)$
MAPBAR	$\overline{\omega(\zeta)}$
MAPBR	$\overline{\omega}(\zeta)$
MAPBR1	$\overline{\omega}(1/\zeta)$
MAPB1	$\omega(1/\zeta)$
MAPPBR	$\overline{\omega'(\zeta)}$
MAPPB1	$\overline{\omega}'(\zeta)$
MAPPB2	$\overline{\omega}'(1/\zeta)$
MAPP1	$\omega''(\zeta)$
MAPP1	$\omega'(\zeta)$
MAP1	$\omega(\zeta)$
MAPB12	$1/\zeta, \omega(1/\zeta), \omega_2(\omega_1(1/\zeta))$
MAPB21	$\overline{\zeta}, \omega(\zeta), \omega_2(\omega_1(\zeta))$
MAPP1	$1, \omega'(\zeta), \omega_2(\omega_1(\zeta)) \omega_1(\zeta)$
MAPPB8	$1, 1, \overline{\omega_2(\omega_1(\zeta))}$
MAPPB8	$1, 1, \omega_2(\omega_1(\zeta))$
MAPP12	$1, \omega'(1/\zeta), \omega_2(\omega_1(1/\zeta)) \omega_1(1/\zeta)$
MAPP21	$1, \omega'(\zeta), \omega_2(\omega_1(\zeta)) \omega_1(\zeta)$
MAPPER	$z, \omega(\zeta), \omega_2(\omega_1(\zeta))$ $z, \omega^{-1}(\zeta), \omega_1^{-1}(\omega_2^{-1}(\zeta))$

Table A-3. FUNCTION COLLOCATION ROUTINES

Subroutine	Function Collocated
PHI	$\alpha f(z)$
PHIB	$\alpha f(\overline{z})$
PHIBP	$\alpha \overline{f}'(z)$
PHIBR	$\alpha f(z)$
PHIB1	$\alpha f(1/\overline{z})$
PHIB1P	$\alpha f'(1/z)$
PHIP	$\alpha f'(z)$
PHIPB	$\alpha \overline{f}'(\overline{z})$
PHIPP	$\alpha f''(z)$
PHIPPB	$\alpha \overline{f}'''(\overline{z})$
PHIBP1	$\alpha f'(z)$
PHIP1B	$\alpha f'(1/\overline{z})$
CONSET	unknown not in $\phi_z$ or $\psi_z$

$\alpha$  is a complex constant and  $f(z)$  is a complex function (usually either  $\phi_z(z)$ ,  $\psi_z(z)$ ,  $\phi(\zeta)$ , or  $\psi(\zeta)$ ).

Table A-4. SPECIALIZED EQUATION GENERATION ROUTINES

Subroutine	Use
FDCOL	Collocation of displacements and forces
STCOL	Collocation of stresses
STITCH	Equate forces and displacements at zone boundaries
COMBIN	Generation of equations for use in combined finite element - MMC analysis

Table A-5. RESULT COMPUTATION ROUTINES

Subroutine	Use
EVAL	Evaluate equation with solution
FDRES	Calculate forces and displacements with solution
STRRES	Calculate stresses with solutions
PRTCOF	Print coefficients solved for
PRTCON	Print unknown found which is not in functions
PRNTMP	Print mapping parameters
PRNTMT	Print material properties
PRNTSR	Print series information
PRTZON	Print all information in zone
KTK2	Calculation of stress intensities

## APPENDIX B. SOURCE LISTINGS FOR MMCLIB

### FUNCTION BRANCH (TH,THBR)

```

C
C
C      FUNCTION TO FIND ANGLE TH+2.*N*PI SUCH THAT
C      THBR < ANGLE < THBR+2.*PI
C
C
COMMON /PIFAC/ PI,HLFPI,TWOP1
TH1=TH
THP=THBR+TWOP1
10 IF (TH1.GE.THBR) GO TO 20
TH1=TH1+TWOP1
GO TO 10
20 IF (TH1.LE.THP) GO TO 30
TH1=TH1-TWOP1
GO TO 20
30 BRANCH=TH1
RETURN
END

```

### SUBROUTINE B4PHDP(XP,YP,IZ,CS2A,SN2A,IREF,A,B)

```

C
C
C      SUBROUTINE TO CALCULATE FUNCTION MULTIPLYING
C      SECOND DERIVATIVE OF PHI IN STRESS EQUATIONS
C
C

```

```

CALL MAPPR(XP,YP,XPR,YPR,IZ)
XBR=0.
YBR=0.
CALL MAPPER(XP,YP,XZBR,YZBR,IZ,1)
YZBR=-YZBR
GO TO (40,10,20),IREF
10 CALL MAPB21(XP,YP,XBR,YBR,IZ)
GO TO 30
20 CALL MAPB12(XP,YP,XBR,YBR,IZ)
30 YBR=-YBR
40 XZBR=XBR-XZER
YZBR=YBR-YZBR
XT=CS2A*XZBR-SN2A*YZBR
YT=CS2A*YZBR+SN2A*XZBR
XT1=XPR*XPR-YPR*YPR
YT1=2.*XPR*YPR
DENOM=1./(XT1*XT1+YT1*YT1)
A=DENOM*(XT*XT1+YT*YT1)
B=DENOM*(XT1*YT-YT1*XT)
RETURN
END

```

### SUBROUTINE B4PHIP (XP,YP,IZ,IOPT,C2,A,B)

```

C
C
C      SUBROUTINE TO CALCULATE FUNCTION MULTIPLYING COMPLEX
C      CONJUGATE OF DERIVATIVE OF PHI IN FORCE,DISPLACEMENT
C      EQUATIONS
C      IOPT
C
C      1 - NO REFLECTION
C      2 - X-AXIS REFLECTION
C      3 - UNIT CIRCLE REFLECTION
C
C

```

```

COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
CALL MAPPER (XP,YP,ZX,ZY,IZ,1)
GO TO (40,10,20,60), IOPT
10 CALL MAPB21 (XP,YP,ZXB,ZYB,IZ)
GO TO 30
20 CALL MAPB12 (XP,YP,ZXB,ZYB,IZ)
30 ZX=ZX-ZXB
ZY=ZY-ZYB
40 XPR1=1.
YPR1=0.
IF (IMAP(IZ,1).EQ.0) GO TO 50
CALL MAPPBR (XP,YP,IZ,1,XPR1,YPR1)
50 CALL MAPPRB (XP,YP,XPR2,YPR2,IZ)
DENOM=C2/((XPR1*XPR2+YPR1*YPR1)*(XPR2*XPR2+YPR2*YPR2))
ZXB=XPR1*XPR2-YPR1*YPR2
ZYB=-XPR1*YPR2-XPR2*YPR1
A=(ZX*ZXB-ZY*ZYB)*DENOM
B=(ZY*ZXB+ZX*ZYB)*DENOM
RETURN
60 A=C2*ZX
B=C2*ZY
RETURN
END

```

```

SUBROUTINE B4PHP(XP,YP,CS2A,SN2A,IZ,IREF,A,B)

```

```

C
C
C          SUBROUTINE TO CALCULATE FUNCTION MULTIPLYING
C          DERIVATIVE OF PHI IN STRESS EQUATIONS
C
C
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
A=0.
B=0.
IF(IMAP(IZ,1).NE.0)GO TO 20
IF(IREF.EQ.1)GO TO 80
X2=1.
Y2=0.
IF(IREF.EQ.2)GO TO 10
XT=XP*XP-YP*YP
YT=2.*XP*YP
DENOM=1./(XT*XT+YT*YT)
X2=-XT*DENOM
Y2= YT*DENOM
10 A=X2*CS2A-Y2*SN2A
B=X2*SN2A+Y2*CS2A
GO TO 80
20 CALL MAPPER(XP,YP,X2,Y2,IZ,1)
Y2=-Y2
CALL MAPPR(XP,YP,DERX,DERY,IZ)
XT=DERX*(DERX+DERX-3.*DERY*DERY)
YT=DERY*(3.*DERX+DERX-DERY*DERY)
DENOM=1./(XT*XT+YT*YT)
DX=XT*DENOM
DY=-YT*DENOM
CALL MAPPP1(XP,YP,IZ,1,X1,Y1)
IF(IMAP(IZ,2).EQ.0)GO TO 30
XT=X1
YT=Y1
CALL MAPPRP(XP,YP,XT1,YT1,IZ)
X1=XT*XT1-YT*YT1
Y1=XT*YT1+YT*XT1
CALL MAPP1(XP,YP,IZ,1,XT1,YT1)
XT=XT1+XT1-YT1*YT1
YT=2.*XT1*YT1
CALL MAP1(XP,YP,IZ,1,WX,WY)

```

```

CALL MAPPP1(WX,WY,IZ,2,XT1,YT1)
X1=X1+XT*XT1-YT*YT1
Y1=Y1+XT*YT1+YT*XT1
30 X3=0.
Y3=0.
GO TO (70,40,50),IREF
40 CALL MAPB21(XP,YP,XT,YT,IZ)
YT=-YT
CALL MAPP21(XP,YP,XT1,YT1,IZ)
GO TO 60
50 CALL MAPP12(XP,YP,XT,YT,IZ)
WX=XP*XP-YP*YP
WY=2.*XP*YP
DENOM=1./(WX*WX+WY*WY)
XT1=-DENOM*(WX*XT+WY*YT)
YT1=-DENOM*(WX*YT-WY*XT)
CALL MAPB12(XP,YP,XT,YT,IZ)
YT=-YT
60 X2=X2-XT
Y2=Y2-YT
CALL MAPPR(XP,YP,XT,YT,IZ)
X3=XT*XT1-YT*YT1
Y3=XT*YT1+YT*XT1
70 XT=X2*XI-Y2*Y1+X3
YT=X2*Y1+Y2*X1+Y3
XT1=DX*XT-DY*YT
YT1=DX*YT+DY*XT
A=CS2A*XT1-SN2A*YT1
B=CS2A*YT1+SN2A*XT1
80 RETURN
END

```

SUBROUTINE COMBIN (NFILE,IZ,IREF,IPRT,IERR)

```

C ROUTINE TO WRITE EQUATIONS FOR
C COMBINED FINITE ELEMENT - MMC
C ANALYSIS
C
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /MAT/ G(5),ETAM(5)
COMMON /MMCFE/ X(150),Y(150),FDRHS(300),EQNS(120,176),
*              KUV(120,2)
DIMENSION RHS(1)
REAL KUV
EQUIVALENCE (RHS(1),FDRHS(1))
DATA NEQ /100/
ICNT=ICNT+1
IF (IERR.NE.0.AND.ICNT.EQ.1) GO TO 70
DO 10 I=1,NEQ
DO 10 J=1,176
10 EQNS(I,J)=0.
REWIND NFILE
READ (NFILE) N1,N2,IDOFS
IF (IPRT.EQ.2.AND.IERR.EQ.0) PRINT 120,N1,N2
NODST=(IDOFS+1)/2
NPT=N2/2
NODLST=NPT+NODST-1
READ (NFILE) (X(I),Y(I),I=1,NPT)
READ (NFILE) (RHS(I),I=1,N1)
DO 50 N=1,NPT
CALL MAPPER(XP,YP,X(N),Y(N),IZ,2)
IF (IPRT.NE.2.OR.IERR.NE.0) GO TO 20
NODE=N+NODST-1
PRINT 130, NODE,X(N),Y(N),XP,YP
20 CALL ZERO (0,0,1,2,1,0)
CALL PTCOL (XP,YP,IZ,2,IREF,1.,1,2,1,2)

```

```

IF (IREF.EQ.4) CALL MLTDSP (XP,YP,IZ)
DO 30 J=1,2
30 READ (NFILE) (KUV(I,J),I=1,N1)
DO 40 I=1,N1
DO 40 J=1,NUNK
40 EQNS(I,J)=EQNS(I,J)+KUV(I,1)*EQUTOT(1,J)+KUV(I,2)*EQUTOT(2,J)
50 CONTINUE
TWOG=2.*G(IZ)
DO 60 I=1,N1
60 EQNS(I,NN)=RHS(I)*TWO
IF (IPRT.GT.0.AND.IERR.EQ.0) PRINT 140, N1,NODST,NODLST
70 N1HLF=N1/2
DO 100 N=1,N1HLF
IE2=2*N
IE1=IE2-1
DO 80 I=1,NN
EQUTOT(1,I)=EQNS(IE1,I)
80 EQUTOT(2,I)=EQNS(IE2,I)
IF (IERR.NE.0) GO TO 90
CALL SAVE (1)
GO TO 100
90 CALL EVAL (1,2,2,XER,YER)
PRINT 110, XER,YER
100 CONTINUE
RETURN
110 FORMAT (1H ,2F10.4)
120 FORMAT (////SH N1 =,I5,10X,4HN2 =,I5
*          ////36H EQUATIONS FOR COMBINED METHOD TAKEN,
1          28H FROM FOLLOWING NODAL POINTS//2X,4HNODE,11X,
2          1HX,11X,1HY)
130 FORMAT (1H ,I5,4E12.4)
140 FORMAT (////I6,33H EQUATIONS GENERATED ON INTERFACE/
*          9H AT NODES,I5,5H THRU,I5)
END

```

```

SUBROUTINE CONINF(ICONST,IRLIM)
C
C
C      SUBROUTINE TO SET UP FOR EXTRA UNKNOWN'S SUCH AS FORCE CONSTAN
C      ICONST - NUMBER OF EXTRA UNKNOWN
C      IRLIM  - TWO DIGIT NUMBER
C
C          01 -- UNKNOWN HAS ONLY IMAG PART
C          10 -- UNKNOWN HAS ONLY REAL PART
C          11 -- UNKNOWN HAS BOTH REAL, IMAG PARTS
C
C
C      DIMENSION IIMRL(2)
C      EQUIVALENCE (IRL,IIMRL(2)),(IIM,IIMRL(1))
C      COMMON /CONST/ ICON(5,2),ISTR(5)
C      COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*                      SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C      CALL DECODE(IRLIM,2,IIMRL,NDUM)
C      IF(IRL.GT.0)IRL=1
C      IF(IIM.GT.0)IIM=1
C      NADD=IRL+IIM
C      IF(NADD.LE.0)GO TO 10
C      ICON(ICONST,1)=IRL
C      ICON(ICONST,2)=IIM
C      ISTR(ICONST)=NUNK+1
C      NUNK=NUNK+NADD
C      NN=NUNK+1
10    RETURN
END

```

```

C SUBROUTINE CONSET(ICNST,XR1,XR2,XI1,XI2)
C
C SUBROUTINE TO SET VALUES FOR COLLOCATION OF ADDED UNKNOWNS
C ICNST - ADDED UNKNOWN NUMBER
C XR1 - VALUE FOR REAL EQUATION, REAL PART OF UNKNOWN
C XR2 - VALUE FOR REAL EQUATION, IMAG PART OF UNKNOWN
C XI1 - VALUE FOR IMAG EQUATION, REAL PART OF UNKNOWN
C XI2 - VALUE FOR IMAG EQUATION, IMAG PART OF UNKNOWN
C
C COMMON /CONST/ ICON(5,2),ISTR(5)
C COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
* SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C I1=ISTR(ICNST)
C IF(ICON(ICNST,1).LE.0)GO TO 10
C EQUTOT(1,I1)=XR1
C EQUTOT(2,I1)=XI1
C I1=I1+1
10 IF(ICON(ICNST,2).LE.0)GO TO 20
C EQUTOT(1,I1)=XR2
C EQUTOT(2,I1)=XI2
20 RETURN
END

```

```

C SUBROUTINE CRSMLT
C
C SUBROUTINE TO READ EQUATIONS FROM TAPE AND PERFORM
C SCALING, CROSS MULTIPLICATION
C
C COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
* SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
C REWIND IUNIT
C DO 40 I=1,NWRT
C READ (IUNIT) ((EQUTOT(J,K),K=1,NN),J=1,2)
C DO 10 J=1,2
C DO 10 K=1,NUNK
10 EQUTOT(J,K)=EQUTOT(J,K)*SCALE(K)
C DO 30 L=1,2
C IND=0
C DO 20 J=1,NUNK
C DO 20 K=J,NUNK
C IND=IND+1
20 A(IND)=A(IND)+EQUTOT(L,J)*EQUTOT(L,K)
C DO 30 J=1,NUNK
30 PHI(J)=PHI(J)+EQUTOT(L,J)*EQUTOT(L,NN)
40 CONTINUE
RETURN
END

```

```

C SUBROUTINE DECODE(IOPT,MAX,IDIGIT,NUM)
C ROUTINE TO SEPARATE DIGITS FROM
C INTEGER CONTAINING STRING OF DIGITS
C
C DIMENSION IDIGIT(1)
C NUM=0
C ITSTR=1
C DO 10 I=1,MAX
10 IDIGIT(I)=0
C DO 20 I=1,MAX
C IF(ITSTR.GT.IOPT)GO TO 30

```

```

NUM=NUM+1
IDEN=ITSTR
ITSTR=10**I
20 IDIGIT(I)=MOD(IOPT,ITSTR)/IDEN
30 RETURN
END

```

```
C SUBROUTINE DOF(NDOF)
C
C ROUTINE TO INTERROGATE MMCLIB DATA BLOCKS
C FOR NUMBER OF UNKNOWNS
C
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C
NDOF=NUNK
RETURN
END
```

```

IF (IREF.EQ.4) CALL MAPPR (XP(I),YP(I),A,B,IZ)
FACT=1./(A*A+B*B)
IF (IOPT.EQ.2) FACT=FACT/(2.*G(IZ))
CALL EVAL (1,2,1,V1,V2)
VALX=(V1*A-V2*B)*FACT
VALY=(V1*B+V2*A)*FACT
40 PRINT 70, VALX,VALY,X(I),Y(I),XP(I),YP(I)
RETURN
50 FORMAT (21HOEVALUATION OF FORCES / 9X,2HF1,11X,2HF2,12X,1HX,12X,1H
1Y     8X,8HX(PARAM),5X,8HY(PARAM) )
60 FORMAT (28HOEVALUATION OF DISPLACEMENTS / 10X,1HU,12X,1HV,12X,1HX,
1     12X,1HY,8X,8HX(PARAM),5X,8HY(PARAM) )
70 FORMAT (1X,6E13.5)
END

```

```

SUBROUTINE FDCOL (XP,YP,N,IZ,IOPT,IREF,RHS1,RHS2,IERR)

```

```

C
C
C      SUBROUTINE TO COMPUTE FORCE, DISPLACEMENT EQUATIONS
C      MEANING OF IREF
C      1 - NO REFLECTIONS
C      2 - X-AXIS REFLECTION
C      3 - UNIT CIRCLE REFLECTION
C
C

```

```

DIMENSION XP(1), YP(1), RHS1(1), RHS2(1)
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
PRINT 40
A=1.
B=0.
DO 20 I=1,N
CALL ZERO (0,0,1,2,1,0)
CALL PTCOL (XP(I),YP(I),IZ,IOPT,IREF,1.,1,2,1,2)
IF(IREF.EQ.4)CALL MAPPR(XP(I),YP(I),A,B,IZ)
EQUTOT(1,NN)=A*RHS1(I)+B*RHS2(I)
EQUTOT(2,NN)=A*RHS2(I)-B*RHS1(I)
IF (IERR.EQ.1) GO TO 10
CALL SAVE (1)
GO TO 20
10 CALL EVAL (1,2,2,XER,YER)
PRINT 30, XER,YER,XP(I),YP(I)
20 CONTINUE
RETURN
30 FORMAT (1H ,2F10.4,2E10.4)
40 FORMAT(1H )
END

```

```

SUBROUTINE FNDMAT

```

```

C
C
C      SUBROUTINE TO SCALE, CROSS-MULTIPLY, AND SOLVE
C      FOR COEFFICIENTS
C
C

```

```

COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
CALL SLVINT
CALL SCLFIX
CALL CRSMLT
CALL SOLVE
DO 10 I=1,NUNK
10 PHI(I)=PHI(I)*SCALE(I)
RETURN
END

```

C  
C SUBROUTINE INIT  
C  
C

C SUBROUTINE TO INITIALIZE ALL COMMON VARIABLES  
C  
C

```
COMMON /CONST/ ICON(5,2),ISTR(5)
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
COMMON /MAT/ G(5),ETAM(5)
COMMON /PIFAC/ PI,MLFPI,TWOP
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                 NPOS(10),IZRO(10),IODRL(10),
*                 IODIM(10),IEVRL(10),IEVIM(10)
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
PI=3.14159265
MLFPI=1.57079633
TWOP=6.28318531
IUNIT=7
ISHFT=0
DO 10 I=1,10
IBEGI(I)=0
IENDI(I)=0
NNEG(I)=0
NPOS(I)=0
IZRO(I)=0
IODRL(I)=0
IODIM(I)=0
IEVRL(I)=0
IEVIM(I)=0
XNOT(I)=0.
10 YNOT(I)=0.
DO 20 I=1,5
ISTR(1)=0
G(I)=0.
ETAM(I)=0.
DO 20 J=1,2
IMAP(I,J)=0
ICON(I,J)=0
DO 20 K=1,5
20 PARAM(I,J,K)=0.
REWIND IUNIT
IZONES=0
NWRT=0
NUNK=0
NUNKS=0
NN=0
DO 30 I=1,175
30 SCALE(I)=0.
RETURN
END
```

C  
C SUBROUTINE K1K2(XP,YP,A,B,K1,K2,IZ)  
C  
C

ROUTINE TO COMPUTE STRESS  
INTENSITY FACTORS

```
REAL K1,K2
CALL ZERO(1,2,1,2,3,0)
CALL PHIPB(XP,YP,A,-B,IZ)
CALL PLACE(IZ,1,2,1,2,1.)
CALL EVAL(1,2,1,K1,K2)
RETURN
END
```

Army Materials and Mechanics Research Center  
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111us-tables, D/A Project 1T161101A91A  
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```

C          SUBROUTINE MAP (XP,YP,P1,P2,P3,P4,P5,M,X,Y)
C
C          SUBROUTINE TO CALCULATE MAPPING FUNCTIONS
C
C          GO TO (10,20), M
C
C          MAPPING #1
C
10 CSPHI=COS(P3)
    SNPHI=SIN(P3)
    RSQ=XP*XP+YP*YP
    RSQS=RSQ+1.
    RSQD=RSQ-1.
    SUM1=(P1*RSQS+P2*RSQD)*XP
    SUM2=(P1*RSQD+P2*RSQS)*YP
    DENOM=1./(2.*RSQ)
    X=P4+(CSPHI*SUM1-SNPHI*SUM2)*DENOM
    Y=P5+(SNPHI*SUM1+CSPHI*SUM2)*DENOM
    GO TO 30
C
C          MAPPING #2
C
20 CSPHI=COS(P3)
    SNPHI=SIN(P3)
    SNHY=SINH(YP)
    CSHY=COSH(YP)
    SUM1=SIN(XP)*(P2*SNHY+P1*CSHY)
    SUM2=COS(XP)*(P2*CSHY+P1*SNHY)
    X=P4+CSPHI*SUM1-SNPHI*SUM2
    Y=P5+SNPHI*SUM1+CSPHI*SUM2
30 RETURN
END

SUBROUTINE MAPB (XP,YP,I2,I12,X,Y)
CALL PARA (I2,I12,M,P1,P2,P3,P4,P5)
CALL MAP (XP,-YP,P1,P2,P3,P4,P5,M,X,Y)
RETURN
END

SUBROUTINE MAPBAR (XP,YP,I2,I12,X,Y)
CALL PARA (I2,I12,M,P1,P2,P3,P4,P5)
CALL MAP (XP,YP,P1,P2,P3,P4,P5,M,X,Y)
Y=-Y
RETURN
END

SUBROUTINE MAPBR (XP,YP,I2,I12,X,Y)
CALL PARA (I2,I12,M,P1,P2,P3,P4,P5)
GO TO (10,20), M
10 BB=P2
GO TO 30
20 BB=-P2
30 CALL MAP (XP,YP,P1,BB,P3,P4,-P5,M,X,Y)
RETURN
END

SUBROUTINE MAPBR1 (XP,YP,I2,I12,X,Y)
CALL MAPB1 (XP,YP,I2,I12,X,Y)
Y=-Y
RETURN
END

```

```

SUBROUTINE MAPB1 (XP,YP,IZ,I12,X,Y)
CALL PARA (IZ,I12,M,P1,P2,P3,P4,P5)
R1=1./ (XP*XP+YP*YP)
XT=XP*R1
YT=YP*R1
CALL MAP (XT,YT,P1,P2,P3,P4,P5,M,X,Y)
RETURN
END

```

```

SUBROUTINE MAPB12 (XP,YP,X,Y,IZ)
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
R1=1./(XP*XP+YP*YP)
X=XP*R1
Y=YP*R1
IF (IMAP(IZ,1).EQ.0) RETURN
CALL MAPB1 (XP,YP,IZ,1,X,Y)
IF (IMAP(IZ,2).EQ.0) RETURN
XX=X
YY=Y
CALL MAP1 (XX,YY,IZ,2,X,Y)
RETURN
END

```

```

SUBROUTINE MAPB21 (XP,YP,X,Y,IZ)
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
X=XP
Y=-YP
IF (IMAP(IZ,1).EQ.0) RETURN
CALL MAPB (XP,YP,IZ,1,X,Y)
IF (IMAP(IZ,2).EQ.0) RETURN
XX=X
YY=Y
CALL MAP1 (XX,YY,IZ,2,X,Y)
RETURN
END

```

SUBROUTINE MAPINF (IZ,M1,P11,P12,P13,P14,P15,M2,P21,P22,  
1 P23,P24,P25)

SUBROUTINE TO SET MAPPING FUNCTION VARIABLES

```
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
DATA ANGCON /.17453292E-1/
IF (M1.LE.0) RETURN
PARAM(IZ,1,1)=P11
PARAM(IZ,1,2)=P12
PARAM(IZ,1,3)=P13*ANGCON
PARAM(IZ,1,4)=P14
PARAM(IZ,1,5)=P15
IMAP(IZ,1)=M1
IF (M2.LE.0) RETURN
PARAM(IZ,2,1)=P21
PARAM(IZ,2,2)=P22
PARAM(IZ,2,3)=P23*ANGCON
PARAM(IZ,2,4)=P24
PARAM(IZ,2,5)=P25
IMAP(IZ,2)=M2
RETURN
END
```

```

C          SUBROUTINE MAPP (XP,YP,P1,P2,P3,P4,P5,M,XD,YD)
C
C          ROUTINE TO COMPUTE FIRST DERIVATIVE
C          OF MAPPING FUNCTION
C
C          COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
C          COMMON /PIFAC/ PI,HLFPI,TWOP
C          GO TO (10,20), M
C
C          MAPPING #1
C
10 BMA=P2-P1
    R4=XP=XP+YP*YP
    R4=R4+R4
    R41=1./R4
    FACT1=.5*(BMA*(XP+XP-YP*YP)+R4*(P1+P2))
    FACT2=BMA*XP*YP
    CS=COS(P3)
    SN=SIN(P3)
    XD=R41*(FACT1*CS+FACT2*SN)
    YD=R41*(FACT1*SN-FACT2*CS)
    RETURN
20 CALL MAP (XP,YP,P2,P1,P3-HLFPI,0.,0.,M,XD,YD)
    RETURN
C
C          END

C          SUBROUTINE MAPINV (X,Y,P1,P2,P3,P4,P5,M,XP,YP)
C
C          SUBROUTINE TO CALCULATE MAPPING FUNCTION INVERSES
C
C          COMMON /PIFAC/ PI,HLFPI,TWOP
C          GO TO (10,20), M
C
C          MAPPING #1
C
10 CALL QUADF (P1,P2,P3,P4,P5,X,Y,1,XP,YP)
    RETURN
C
C          MAPPING #2
C
20 IMAPR=2
30 CALL QUADF (P2,-P1,P3+HLFPI,P4,P5,X,Y,IMAPR,XX,YY)
    XP=XX
    YP=YY
    IF (P1.EQ.P2) GO TO 50
    XP=ATAN2(YY,XX)
    YP=- ALOG(SQRT(XX*XX+YY*YY))
    IF (YP.GT.-.0001) GO TO 50
    IF (IMAPR.NE.-2) GO TO 40
    WRITE (6,60) M,X,Y
    STOP
40 IMAPR=-2
    GO TO 30
50 RETURN
60 FORMAT (17H ERROR IN INVERSE ,I3.2E12.5)
    END

C          SUBROUTINE MAPPB1 (XP,YP,IZ,I12,XD,YD)
C          CALL PARA (IZ,I12,M,P1,P2,P3,P4,P5)
C          GO TO (10,20), M
10 CALL MAPP (XP,YP,P1,P2,-P3,P4,P5,M,XD,YD)
    RETURN
20 CALL MAPP (-XP,-YP,P1,P2,-P3,P4,P5,M,XD,YD)
    RETURN
    END

```

```
SUBROUTINE MAPPBR (XP,YP,IZ,I12,XD,YD)
CALL PARA (IZ,I12,M,P1,P2,P3,P4,P5)
CALL MAPP (XP,YP,P1,P2,P3,P4,P5,M,XD,YD)
YD=-YD
RETURN
END
```

```
SUBROUTINE MAPPB2 (XP,YP,IZ,I12,XD,YD)
RR=1./SQRT(XP*XP+YP*YP)
XX=XP*RR
YY=-YP*RR
CALL MAPPB1 (XX,YY,IZ,I12,XD,YD)
RETURN
END
```

```
SUBROUTINE MAPPDP(XP,YP,XD,YD,IZ)
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
XD=1.
YD=0.
IF(IMAP(IZ,1).EQ.0.AND.IMAP(IZ,2).EQ.0)RETURN
CALL MAPPP1(XP,YP,IZ,1,ZMX2,ZMY2)
IF(IMAP(IZ,2).NE.0)GO TO 10
XD=ZMX2
YD=ZMY2
RETURN
10 CALL MAPP1 (XP,YP,IZ,1,ZMX1,ZMY1)
ZMX1SQ=ZMX1-ZMY1*ZMY1
ZMY1SQ=2.*ZMX1*ZMY1
CALL MAPB(XP,-YP,IZ,WXP,WY)
CALL MAPP1 (WX,WY,IZ,2,WMX1,WMY1)
CALL MAPPP1(WX,WY,IZ,2,WMX2,WMY2)
XD=WMX2*ZMX1SQ-WMY2*ZMY1SQ+WMX1*ZMX2-WMY1*ZMY2
YD=WMX2*ZMY1SQ+WMY2*ZMX1SQ+WMX1*ZMY2+WMY1*ZMX2
RETURN
END
```

```
SUBROUTINE MAPPP1 (XP,YP,IZ,I12,XD2,YD2)
CALL PARA (IZ,I12,M,P1,P2,P3,P4,P5)
CALL MAPPP (XP,YP,P1,P2,P3,P4,P5,M,XD2,YD2)
RETURN
END
```

```
SUBROUTINE MAPPR(XP,YP,XD,YD,IZ)
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
XD=1.
YD=0.
IF(IMAP(IZ,1).EQ.0)GO TO 10
CALL MAPP1(XP,YP,IZ,1,XP1,YP1)
CALL MAPPRP(XP,YP,XP2,YP2,IZ)
XD=XP1*XP2-YP1*YP2
YD=XP1*YP2+XP2*YP1
10 RETURN
END
```

SUBROUTINE MAPPER (XP,YP,X,Y,IZ,INV)

```
SUBROUTINE MAPP1 (XP,YP,IZ,I12,XD,YD)
CALL PARA (IZ,I12,M,P1,P2,P3,P4,P5)
CALL MAPP (XP,YP,P1,P2,P3,P4,P5,M,XD,YD)
RETURN
END
```

```

C          SUBROUTINE MAPPP(XP,YP,P1,P2,P3,P4,P5,M,XD2,YD2)
C
C          ROUTINE TO COMPUTE SECOND DERIVATIVE
C          OF MAPPING FUNCTION
C
C          GO TO (10,20), M
C
C          MAPPING #1
C
10     R6=XP*XP+YP*YP
        R6=(P1-P2)/(R6+R6+R6)
        FACT1=XP*XP*XP-3.*XP*YP*YP
        FACT2=YP*YP*YP-3.*YP*XP*XP
        CS=COS(P3)
        SN=SIN(P3)
        XD2=R6*(FACT1*CS-FACT2*SN)
        YD2=R6*(FACT1*SN+FACT2*CS)
        RETURN

C          MAPPING #2

```

C

```
20 CALL MAP (XP,YP,P1,P2,P3,0.,0.,M,XD2,YD2)
  XD2=-XD2
  YD2=-YD2
  RETURN
  END
```

```
SUBROUTINE MAPPRS (XP,YP,XD,YD,IZ)
CALL MAPPRP (XP,YP,XD,YD,IZ)
YD=-YD
RETURN
END
```

```
SUBROUTINE MAPPRP (XP,YP,XD,YD,IZ)
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
XD=1.
YD=0.
IF (IMAP(IZ,1).EQ.0.OR.IMAP(IZ,2).EQ.0) RETURN
CALL MAP1 (XP,YP,IZ,1,XX,YY)
CALL MAPP1 (XX,YY,IZ,2,XD,YD)
RETURN
END
```

```
SUBROUTINE MAPP12(XP,YP,XD,YD,IZ)
DENOM=1. / (XP*XP+YP*YP)
X1=XP-DENOM
Y1=YP-DENOM
CALL MAPPR(X1,Y1,XP,YD,IZ)
YD=-YD
RETURN
END
```

```
SUBROUTINE MAPP21(XP,YP,XD,YD,IZ)
CALL MAPPR(XP,-YP,XD,YD,IZ)
YD=-YD
RETURN
END
```

```
SUBROUTINE MAP1 (XP,YP,IZ,I12,X,Y)
CALL PARA (IZ,I12,M,P1,P2,P3,P4,P5)
CALL MAP (XP,YP,P1,P2,P3,P4,P5,M,X,Y)
RETURN
END
```

```
SUBROUTINE MLTDSP(XP,YP,IZ)
CALL MAPPR(XP,YP,A,B,IZ)
AA=A/(A+A+B+B)
BB=B/(A+A+B+B)
CALL ROTZON(3,IZ,AA,-BB,BB,AA)
RETURN
END
```

```

C SUBROUTINE NWRTFL(N)
C
C SUBROUTINE TO ALTER VARIABLE CONTAINING NUMBER
C OF EQUATIONS WRITTEN ON CURRENT SCRATCH FILE
C
C COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
* NWRT=N
* RETURN
* END

C FUNCTION NWRTSV(IDUM)
C
C FUNCTION TO SAVE NUMBER OF EQUATIONS WRITTEN
C ON CURRENT SCRATCH UNIT
C
C COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
* NWRTSV=NWRT
* RETURN
* END

C SUBROUTINE PARA (IZ,I12,M,P1,P2,P3,P4,P5)
C
C SUBROUTINE TO FIND MAPPING FUNCTION PARAMETERS IN ZONE
C
C COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
M=IMAP(IZ,I12)
P1=PARAM(IZ,I12,1)
P2=PARAM(IZ,I12,2)
P3=PARAM(IZ,I12,3)
P4=PARAM(IZ,I12,4)
P5=PARAM(IZ,I12,5)
RETURN
END

C SUBROUTINE PHI (XP,YP,A,B,IZ)
C
C ROUTINE TO COLLOCATE A FUNCTION IN A ZONE
C
C CALL ZETN (XP,YP,IZ)
CALL SERFIL (IZ,1.,1.,A,B)
RETURN
END

C SUBROUTINE PHIB (XP,YP,A,B,IZ)
CALL PHI (XP,-YP,A,B,IZ)
RETURN
END

C SUBROUTINE PHIBP (XP,YP,A,B,IZ)
CALL ZETN1 (XP,YP,IZ)
CALL SERFIL (IZ,1.,-1.,A,B)
RETURN
END

```

```
SUBROUTINE PHIBP1(XP,YP,A,B,IZ)
CALL PHIP(XP,-YP,A,B,IZ)
RETURN
END
```

```
SUBROUTINE PHIBR(XP,YP,A,B,IZ)
CALL ZETN(XP,YP,IZ)
CALL SERFIL(IZ,-1.,-1.,A,B)
RETURN
END
```

```
SUBROUTINE PHIB1 (XP,YP,A,B,IZ)
R1=1./(XP*XP+YP*YP)
CALL PHI (XP*R1,YP*R1,A,B,IZ)
RETURN
END
```

```
SUBROUTINE PHIB1P(XP,YP,A,B,IZ)
RR=1./(XP*XP+YP*YP)
CALL PHIBP (XP=RR,-YP=RR,A,B,IZ)
RETURN
END
```

```
SUBROUTINE PHIP(XP,YP,A,B,IZ)
C
C      ROUTINE TO COLLOCATE DERIVATIVE
C      OF A FUNCTION
C
CALL ZETN1(XP,YP,IZ)
CALL SERFIL(IZ,1.,1.,A,B)
RETURN
END
```

```
SUBROUTINE PHIPB(XP,YP,A,B,IZ)
CALL ZETN1(XP,YP,IZ)
CALL SERFIL(IZ,-1.,-1.,A,B)
RETURN
END
```

```
SUBROUTINE PHIPP (XP,YP,A,B,IZ)
C
C      ROUTINE TO COLLOCATE SECOND
C      DERIVATIVE OF A FUNCTION IN A ZONE
C
CALL ZETN2 (XP,YP,IZ)
CALL SERFIL (IZ,1.,1.,A,B)
RETURN
END
```

```

SUBROUTINE PHIPPB(XP,YP,A,B,IZ)
CALL ZETN2(XP,YP,IZ)
CALL SERFIL(IZ,-1.,-1.,A,B)
RETURN
END

```

```

SUBROUTINE PHIP1B(XP,YP,A,B,IZ)
RR=1./(XP*XP+YP*YP)
CALL PHIP(XP*RR,YP*RR,A,B,IZ)
RETURN
END

```

SUBROUTINE PLACE (IZ,IE1,IE2,IT1,IT2,WT)

SUBROUTINE TO PUT COEFFICIENTS FROM ZONE EQUATION  
INTO MASTER EQUATION

```

COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
NTRMS=IENDI(IZ)-IBEGI(IZ)+1
ITOT=IE2-IE1+1
DO 10 I=1,ITOT
IE=I+IE1-1
IT=I+IT1-1
DO 10 J=1,NTRMS
J1=J+IBEGI(IZ)-1
10 EQUTOT(IT,J1)=EQUTOT(IT,J1)+EQU(IE,J)*WT
RETURN
END

```

SUBROUTINE POINTF (IZ,X1,Y1,X2,Y2,NPT,NBEG,NNEND,ICTYP,GPAR,  
2 IMAP,INV,X,Y,XPAR,YPAR)

## SUBROUTINE TO FIND POINTS AT WHICH TO COLLOCATE

IZ - ZONE NUMBER  
 X1 + I Y1 - BEGINNING POINT  
 X2 + I Y2 - ENDING POINT  
 NBEG,NNEND - NUMBER OF POINTS TO LEAVE OUT AT  
 BEGINNING,END  
 ICTYP - 1 -- STRAIGHT LINE  
 2 -- CIRCULAR ARC  
 3 -- ELLIPTICAL ARC  
 IMAP - MAP COORDINATES UNLESS 0  
 INV - 1 -- MAPPING FROM PARAMETER  
 2 -- MAPPING TO PARAMETER  
 GPAR(1) - AXIS IN X-DIRECTION( ICTYP=2,3 )  
 GPAR(2) - AXIS IN Y-DIRECTION( ICTYP=2,3 )  
 GPAR(3) - ANGLE OF ROTATION ( ICTYP=3 )  
 GPAR(4) - X0 ( ICTYP=2,3 )  
 GPAR(5) - Y0 ( ICTYP=2,3 )

```
COMMON /PIFAC/ PI,HLPPI,TWOPPI
DIMENSION X(1), Y(1), XPAR(1), YPAR(1), GPAR(1)
DATA ICLOCK /1/
GPAR3R=GPAR(3)*.17453292E-1
XN=NPT-1
```

```

NSTP=NPT-NNEND
GO TO (10,20,30), ICTYP
10 FACT1=(X2-X1)/XN
FACT2=(Y2-Y1)/XN
GO TO 70
20 XX=X1-GPAR(4)
YY=Y1-GPAR(5)
TH1=TANGO(YY,XX)
XX=X2-GPAR(4)
YY=Y2-GPAR(5)
TH2=TANGO(YY,XX)
GO TO 40
30 CALL QUADF (GPAR(1),GPAR(2),GPAR3R,GPAR(4),GPAR(5),X1,Y1,1,XX,YY)
TH1=TANGO(YY,XX)
CALL QUADF (GPAR(1),GPAR(2),GPAR3R,GPAR(4),GPAR(5),X2,Y2,1,XX,YY)
TH2=TANGO(YY,XX)
40 IF (ICLOCK.EQ.-1) GO TO 50
IF (TH2.LT.TH1) TH2=TH2+TWOPI
GO TO 60
50 IF (TH2.GT.TH1) TH2=TH2-TWOPI
60 TH0=.5*(TH1+TH2)+PI
TH0=BRANCH(TH0,-PI)
TH1=BRANCH(TH1,TH0)
TH2=BRANCH(TH2,TH0)
THETA=(TH2-TH1)/XN
70 DO 110 I=1,NPT
IF (I.LE.NBEG.OR.I.GT.NSTP) GO TO 110
XNN=I-1
I1=I-NBEG
GO TO (80,90,90), ICTYP
80 X(I1)=X1+XNN*FACT1
Y(I1)=Y1+XNN*FACT2
GO TO 110
90 ANG=TH1+XNN*THETA
IF (ICTYP.EQ.3) GO TO 100
X(I1)=GPAR(4)+GPAR(1)*COS(ANG)
Y(I1)=GPAR(5)+GPAR(1)*SIN(ANG)
GO TO 110
100 XX=COS(ANG)
YY=SIN(ANG)
CALL MAP (XX,YY,GPAR(1),GPAR(2),GPAR3R,GPAR(4),GPAR(5),
* 1,X(I1),Y(I1))
110 CONTINUE
NPT=NPT-NBEG-NNEND
IF (INV.EQ.2) GO TO 130
DO 120 I=1,NPT
XPAR(I)=X(I)
120 YPAR(I)=Y(I)
130 IF (IMAP.EQ.0) RETURN
DO 140 I=1,NPT
140 CALL MAPPER (XPAR(I),YPAR(I),X(I),Y(I),IZ,INV)
RETURN
END

```

```

SUBROUTINE POWSER(XP,YP,A,B,IZ)
C
C      ROUTINE TO COMPUTE TERMS
C      FOR POWER SERIES
C
COMMON /PIFAC/ PI,HLFPI,TWOPI
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                 NPOS(10),IZRO(10),IODRL(10),
*                 IODIM(10),IEVRL(10),IEVIM(10)
XX=XP-XNOT(IZ)
YY=YP-YNOT(IZ)
IPOW=-NNEG(IZ)

```

```

NTOT1=NNEG(IZ)+NPOS(IZ)+1
ISTRRT=ISHFT+1
R1=SORT(XX*XX+YY*YY)
TH1=ATAN2(YY,XX)
XIPOW=IPOW
R(ISTRRT)=SORT(A*A+B*B)*(R1==IPOW)
TH(ISTRRT)=BRANCH(ATAN2(B,A)+TH1*XIPOW,-PI)
DO 10 I=2,NTOT1
I1=ISHFT+I
R(I1)=R(I1-1)*R1
10 TH(I1)=BRANCH(TH(I1-1)+TH1,-PI)
RETURN
END

```

```

C SUBROUTINE PRNTMP (IZ)
C
C ROUTINE TO PRINT MAPPING
C INFORMATION IN A ZONE
C
COMMON /MAP/ IMAP(5,2),PARAM(5,2,5)
IMP=1
PRINT 20, IZ
IF (IMAP(IZ,1).GT.0) GO TO 10
PRINT 30
RETURN
10 PRINT 40, IMP,IMAP(IZ,1),(PARAM(IZ,1,I),I=1,5)
IF (IMAP(IZ,2).LE.0) RETURN
IMP=2
PRINT 40, IMP,IMAP(IZ,2),(PARAM(IZ,2,I),I=1,5)
RETURN
20 FORMAT (////28H MAPPING FUNCTION PARAMETERS,
1           13H FOR ZONE NO.,I2)
30 FORMAT (28H --NO MAPPING IN THIS ZONE--)
40 FORMAT (21H MAPPING FUNCTION NO.,I2,8H IN ZONE/
1           13H MAPPING TYPE,I2/12H PARAMETERS:,SE12.5/)
END

```

```

C SUBROUTINE PRINTR (IZN)
C
C      ROUTINE TO PRINT COEFFICIENTS
C      OF EITHER A PHI OR PSI FUNCTION
C
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                 NPOS(10),IZRO(10),IODRL(10),
*                 IODIM(10),IEVRL(10),IEVIM(10)
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
DATA ZERO /0./
IZR=IZRO(IZN)
IOR=ICDRL(IZN)
IOI=ICDIM(IZN)
IER=IEVRL(IZN)
IEI=IEVIM(IZN)
PRINT 40
NPA=NNEG(IZN)
NPA=-NPA
NPWRS=NPA+NPOS(IZN)+1
IEO=2
IF (NPA/2.NE.(NPA+1)/2) IEO=1
IND=IBEGI(IZN)
DO 30 I=1,NPWRS
PRTRL=ZERO
PRTIM=ZERO

```

```

IF (NP.EQ.0.AND.IZR.EQ.0) GO TO 20
IF ((IOR.EQ.0.AND.IEO.EQ.1).OR.(IER.EQ.0.AND.IEO.EQ.2)) GO TO 10
PTRL=PHI(IND)
IND=IND+1
10 IF ((IOI.EQ.0.AND.IEO.EQ.1).OR.(IEI.EQ.0.AND.IEO.EQ.2)) GO TO 20
PRTIM=PHI(IND)
IND=IND+1
20 PRINT 50, NP,PTRL,PRTIM
NP=NP+1
IEO=3-IEO
30 CONTINUE
RETURN
40 FORMAT (4H POW,4X,9HREAL COEF,4X,9HIMAG COEF )
50 FORMAT (1H ,I3,2E13.5)
END

```

SUBROUTINE PRINTS (NZ)

```

C ROUTINE TO PRINT INFORMATION ABOUT
C EITHER A PHI OR PSI FUNCTION IN A ZONE
C
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
* NPOS(10),IZRO(10),IODRL(10),
* IODIM(10),IEVRL(10),IEVIM(10)
IF (NZ.GT.5) GO TO 10
PRINT 30, NZ
GO TO 20
10 NNZ=NZ-5
PRINT 40, NNZ
20 NNN=-NNEG(NZ)
IF (NNEG(NZ).GT.0) PRINT 50, NNN
IF (NPOS(NZ).GT.0) PRINT 60, NPOS(NZ)
IF (IZRO(NZ).GT.0) PRINT 70
PRINT 80, IODRL(NZ),IODIM(NZ),IEVRL(NZ),IEVIM(NZ)
RETURN
30 FORMAT (//2H PHI FUNCTION FOR ZONE,I2)
40 FORMAT (//2H PSI FUNCTION FOR ZONE,I2)
50 FORMAT (2H HIGHEST NEGATIVE POWER IS,I4)
60 FORMAT (2H HIGHEST POSITIVE POWER IS,I4)
70 FORMAT (5H ZERO POWER INCLUDED(IF CONSISTENT WITH SYMMETRIES))
80 FORMAT (34H COEFFICIENTS INCLUDED(1=YES,0=NO)/
1           11H ODD POWER,5X,10HEVEN POWER/11H REAL  IMAG,5X,
2           10HREAL  IMAG/1X,I4,I6,5X,I4,I6)
END

```

SUBROUTINE PRNTMT (IZ)

```

C ROUTINE TO PRINT MATERIAL PROPERTIES
C
COMMON /MAT/ G(5),ETAM(5)
PRINT 10, IZ
PRINT 20, G(IZ),ETAM(IZ)
RETURN
10 FORMAT (///3H MATERIAL PARAMETERS FOR ZONE NO.,I2)
20 FORMAT (6H   G =,E12.5/6H ETA =,E12.5)
END

```

SUBROUTINE PRNTSR (IZ)

```

C ROUTINE TO PRINT INFORMATION ON
C ALL SERIES IN A ZONE
C

```

```

COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                      NPOS(10),IZRO(10),IODRL(10),
*                      IODIM(10),IEVRL(10),IEVIM(10)
PRINT 20, IZ
NZ=IZ
DO 10 I=1,2
IF (ISTYP(NZ).LE.0) GO TO 10.
CALL PRINTS (NZ)
10 NZ=NZ+5
RETURN
20 FORMAT (///32H SERIES INFORMATION FOR ZONE NO.,I2)
END

```

```

C          SUBROUTINE PRTCOP (IOPT)
C          SUBROUTINE TO PRINT COEFFICIENTS OF
C          PHI AND PSI FUNCTIONS IN VARIOUS ZONES
C          IOPT - INTEGER CONTAINING ZONE NUMBERS
C
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                      NPOS(10),IZRO(10),IODRL(10),
*                      IODIM(10),IEVRL(10),IEVIM(10)
DIMENSION IZONE(5)
CALL DECODE (IOPT,5,IZONE,NNZ)
IF (NNZ.EQ.0) RETURN
PRINT 50
DO 20 I=1,NNZ
NZ=IZONE(NNZ-1+1)
IF (NPOS(NZ).LE.0.AND.NNEG(NZ).LE.0) GO TO 10
ISER=ISTYP(NZ)
PRINT 30, NZ
PRINT 60, ISER
CALL PRINTR (NZ)
10 NZ=NZ+5
IF (NPOS(NZ).LE.0.AND.NNEG(NZ).LE.0) GO TO 20
ISER=ISTYP(NZ)
PRINT 40
PRINT 60, ISER
CALL PRINTR (NZ)
20 CONTINUE
RETURN
30 FORMAT (///9H ZONE NO.,I2//13H PHI FUNCTION )
40 FORMAT (//13H PSI FUNCTION )
50 FORMAT (////34H COEFFICIENTS IN PHI,PSI FUNCTIONS )
60 FORMAT (12H SERIES TYPE,I2/)
END

```

```

C          SUBROUTINE PRTCON (IOPT)
C          ROUTINE TO PRINT EXTRA PARAMETERS
C          IOPT - VARIABLE CONTAINING PARAMETER NUMBERS
C
COMMON /CONST/ ICON(5,2),ISTR(5)
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
DIMENSION IPRT(5)
CALL DECODE (IOPT,5,IPRT,NC)
IF (NC.EQ.0) GO TO 40
DO 30 I=1,NC
IC=IPRT(NC-I+1)
IF (ICON(IC,1).EQ.0.AND.ICON(IC,2).EQ.0) GO TO 30
CONRL=0.
CONIM=0.
I1=ISTR(1)
IF (ICON(IC,1).EQ.0) GO TO 10

```

```

CONRL=PHI(I1)
I1=I1+1
10 IF (ICON(IC,2).EQ.0) GO TO 20
CONIM=PHI(I1)
20 PRINT 50, IC,CONRL,CONIM
30 CONTINUE
40 RETURN
50 FORMAT (///20H EXTRA PARAMETER NO.,I2/1X,2E13.5)
END

```

```

SUBROUTINE PRTZON (IOPT)
C
C      ROUTINE TO PRINT ALL INFORMATION IN ZONE
C      IOPT - VARIABLE CONTAINING ZONE NUMBERS
C
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                  NPOS(10),IZRO(10),IODRL(10),
*                  IODIM(10),IEVRL(10),IEVIM(10)
DIMENSION IZONE(5)
CALL DECODE (IOPT,5,IZONE,NNZ)
IF (NNZ.EQ.0) RETURN
PRINT 20
DO 10 I=1,NNZ
IZ=IZCNE(NNZ-I+1)
IF (IZ.GT.5.OR.ISTYP(IZ).LE.0.AND.ISTYP(IZ+5).LE.0) RETURN
CALL PRNTSR (IZ)
CALL PRNTMT (IZ)
10 CALL PRNTMP (IZ)
RETURN
20 FORMAT (1H1)
END

```

```

SUBROUTINE PTCOL (XP,YP,I2,IOPT,IREF,WT,IF1,IF2,IT1,IT2)
C
C      SUBROUTINE TO COLLOCATE AT ONE POINT EITHER FORCES
C      OR DISPLACEMENTS
C
C      IOPT      - 1--COLLOCATE FORCES
C                  2--COLLOCATE DISPLACEMENTS
C      IREF      - 1--NO REFLECTIONS
C                  2--X-AXIS REFLECTION
C                  3--UNIT CIRCLE REFLECTION
C      WT        - WEIGHTING OF EQUATIONS
C      IF1,IF2   - WHICH EQUATIONS TO SAVE
C      IT01,IT02- WHERE TO PLACE EQUATIONS TO BE SAVED
C                  IN MASTER EQUATIONS(EITHER 1ST OR 2ND EQUAT
C
COMMON /MAT/ G(5),ETAM(5)
C1=1.
C2=1.
IF (IOPT.EQ.1) GO TO 10
C1=ETAM(I2)
C2=-1.
10 CALL ZERO (1,2,0,0,0,0)
CALL B4PHIP (XP,YP,I2,IREF,C2,A,B)
CALL PHIPB (XP,YP,A,B,I2)
A=1.
B=0.
IF(IREF.EQ.4)CALL MAPPR(XP,YP,A,B,I2)
CALL PHI (XP,YP,C1*A,-C1*B,I2)
GO TO (40,20,30,40), IREF
20 CALL PHIB (XP,YP,-C2,0.,I2)

```

```

GO TO 40
30 CALL PHIB1 (XP,YP,-C2,0.,IZ)
40 CALL PLACE (IZ,IF1,IF2,IT1,IT2,WT)
IF (IREF.EQ.2.OR.IREF.EQ.3) GO TO 50
CALL ZERO (1,2,0,0,0,0)
CALL PHIBR (XP,YP,C2,0.,IZ+5)
CALL PLACE (IZ+5,IF1,IF2,IT1,IT2,WT)
50 RETURN
END

```

```

SUBROUTINE PWSERD(XP,YP,A,B,IZ)
C
C      COMPUTER TERMS IN DERIVATIVE
C      OF POWER SERIES
C
COMMON /PIFAC/ PI,HLFPI,TWOP
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                  NPOS(10),IZRO(10),IODRL(10),
*                  IODIM(10),IEVRL(10),IEVIM(10)
NTOT1=NNEG(IZ)+NPOS(IZ)+1
IPOW=-NNEG(IZ)
XX=XP-XNOT(IZ)
YY=YP-YNOT(IZ)
XIPOW=IPOW
RHOAB=SQRT(A*A+B*B)
IF(RHOAB.NE.0.)PHIAB=ATAN2(B,A)
R1=SQRT(XX*XX+YY*YY)
TH1=ATAN2(YY,XX)
DO 10 I=1,NTOT1
I1=ISHFT+I
XIPOW=IPOW
R(I1)= RHOAB*XIPOW*(R1*(IPOW-1))
TH(I1)=BRANCH(PHIAB+(XIPOW-1.)*TH1,-PI)
IF(IPOW.GE.0)GO TO 10
R(I1)=-R(I1)
TH(I1)=BRANCH(TH(I1)+PI,-PI)
10 IPOW=IPOW+1
RETURN
END

```

```

SUBROUTINE QUADF (A,B,PHI,X0,Y0,XM,YM,IMAP,XQ,YQ)
C
C      SUBROUTINE USED BY INVERSE MAPPINGS TO COMPUTE SQUARE ROOT
C      OF FUNCTION OF THE FORM (Z*Z -C*C) -- C IS REAL
C
COMMON /PIFAC/ PI,HLFPI,TWOP
EQUIVALENCE (PIH,HLFPI), (PIT,TWOP)
DENOM=A+B
X1=XM-X0
Y1=YM-Y0
IF (DENOM.EQ.0) GO TO 50
DENOM=1./DENOM
FACT=1.
IF (IMAP.EQ.-2) FACT=-1.
ICT=0
CS=COS(PHI)
SN=SIN(PHI)
XZ=X1*CS+Y1*SN
YZ=Y1*CS-X1*SN
XC=0.

```

```

YC=0.
AA=A*A
BB=B*B
IF (AA.GT.BB) XC=SQRT(AA-BB)
IF (BB.GT.AA) YC=SQRT(BB-AA)
X1=XZ+XC
Y1=YZ+YC
R1=SQRT(X1*X1+Y1*Y1)
TH1=0.
IF (X1.EQ.0..AND.Y1.EQ.0.) GO TO 10
TH1=ATAN2(Y1,X1)
IF (BB.GT.AA) TH1=BRANCH(TH1,-3.*PI)
10 X1=XZ-XC
Y1=YZ-YC
R2=SQRT(X1*X1+Y1*Y1)
TH2=0.
IF (X1.EQ.0..AND.Y1.EQ.0.) GO TO 20
TH2=ATAN2(Y1,X1)
IF (BB.GT.AA) TH2=BRANCH(TH2,-PI)
IF (AA.GT.BB) TH2=BRANCH(TH2,0.)
20 X2=SQRT(R1+R2)
Y2=.5*(TH1+TH2)
30 XQ=DENOM*(X2+FACT*X2*COS(Y2))
YQ=DENOM*(Y2+FACT*X2*SIN(Y2))
XX=XQ+XQ+YQ+YQ
IF (XX.GT..9999.OR.IABS(IMAP).EQ.2) RETURN
IF (ICT.NE.1) GO TO 40
WRITE (6,60) XM,YM
STOP
40 FACT=-FACT
ICT=1
GO TO 30
50 XQ=ATAN2(Y1,X1)
IF (XQ.GT.PHI+PI) XQ=XQ-PI
IF (XQ.LT.PHI-PI) XQ=XQ+PI
XQ=PHI-XQ
YQ= ALOG(SQRT(X1*X1+Y1*Y1)/A)
RETURN
60 FORMAT (15H ERROR IN QUADF,10X,3HXM=,E12.4,5X,3HXM=,E12.4)
END

```

SUBROUTINE PWSRD2(XP,YP,A,B,IZ)

```

C ROUTINE TO COMPUTE TERMS IN
C SECOND DERIVATIVE OF POWER SERIES
C
COMMON /PIFAC/ PI,HLFPI,TWOP
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                 NPOS(10),IZRO(10),IODRL(10),
*                 IODIM(10),IEVRL(10),IEVIM(10)
NTOT1=NNEG(IZ)+NPOS(IZ)+1
IPOW=-NNEG(IZ)
XX=XP-XNOT(IZ)
YY=YP-YNOT(IZ)
R1=SQRT(XX*XX+YY*YY)
TH1=ATAN2(YY,XX)
RHOAB=SQRT(A*A+B*B)
PHIAB=ATAN2(B,A)
DO 10 I=1,NTOT1
XIPOW=IPOW-2
RFACT=IPOW*(IPOW-1)
I1=ISHFT+1
R(I1)=RHOAB*RFACT*(R1***(IPOW-2))
TH(I1)=BRANCH(PHIAB+XIPOW*TH1,-PI)
10 IPOW=IPOW+1
RETURN
END

```

```

C SUBROUTINE RADD (RR,TT,NTRMS)
C
C      ADD SERIES OF COMPLEX NUMBERS IN POLAR FORM
C
COMMON /POWERS/ R(100),TH(100),ISHFT
DIMENSION RR(1), TT(1)
DO 30 I=1,NTRMS
I1=ISHFT+I
XX=RR(I1)*COS(TT(I1))+R(I1)*COS(TH(I1))
YY=RR(I1)*SIN(TT(I1))+R(I1)*SIN(TH(I1))
IF (XX.NE.0..OR.YY.NE.0.) GO TO 10
R(I1)=0.
TH(I1)=0.
GO TO 30
10 TH(I1)=ATAN2(YY,XX)
IF (ABS(COS(TH(I1))).LT..1) GO TO 20
R(I1)=XX/COS(TH(I1))
GO TO 30
20 R(I1)=YY/SIN(TH(I1))
30 CONTINUE
RETURN
END

SUBROUTINE RHS (IOPT,NPT,X,Y,X1,Y1,X2,Y2,RHS10,RHS20,SIG0,SIG1,
1           RHS1,RHS2)
C
C      ROUTINE TO COMPUTE VALUES OF F1 + I F2
C      MEANING OF IOPT
C      1 - CONSTANT VALUE
C      2 - LINEARLY VARYING NORMAL STRESS, STRAIGHT BOUNDARY
C      3 - LINEARLY VARYING SHEAR STRESS, STRAIGHT BOUNDARY
C      4 - CONSTANT NORMAL STRESS, CIRCULAR, ELLIPTICAL BOUNDARY
C      5 - CONSTANT SHEAR STRESS, CIRCULAR, ELLIPTICAL BOUNDARY
C
COMMON /PIFAC/ PI,HLFPI,TWOP
DIMENSION X(1), Y(1), RHS1(1), RHS2(1)
C1=0.
C2=0.
C3=0.
C4=0.
GO TO (90,10,20,60,70), IOPT
10 C1=1.
C2=1.
GO TO 30
20 C3=1.
C4=1.
30 THETAC=ATAN2(Y2-Y1,X2-X1)
IF (ABS(THETAC-HLFPI).GT..00001) GO TO 40
CSINV=1.
GO TO 90
40 IF (ABS(THETAC+HLFPI).GT..00001) GO TO 50
CSINV=-1.
GO TO 90
50 CSINV=1./COS(THETAC)
GO TO 90
60 C1=1.
GO TO 80
70 C3=1.
80 CSINV=1.
90 DO 100 I=1,NPT
XSQDIF=.5*(X(I)*X(I)-X1*X1)+SIG1*CSINV
YSQDIF=.5*(Y(I)*Y(I)-Y1*Y1)+SIG1*CSINV
XDIFF=(X(I)-X1)*SIG0
YDIFF=(Y(I)-Y1)*SIG0
RHS1(I)=RHS10+C1*XDIFF+C2*XSQDIF-C3*YDIFF-C4*YSQDIF
RHS2(I)=RHS20+C1*YDIFF+C2*YSQDIF+C3*XDIFF+C4*XSQDIF
100 CONTINUE
RETURN
END

```

```

C SUBROUTINE ROTEQU (IOPT,IZNS,A1,A2,A3,A4)
C
C      MULTIPLY EQUATIONS IN GIVEN
C      ZONES BY COMPLEX CONSTANTS
C
C      DIMENSION IZ(5)
C      CALL DECODE (IZNS,5,IZ,MAX)
C      IF (MAX.LE.0) RETURN
C      DO 10 I=1,MAX
C 10 CALL ROTZON (IOPT,IZ(I),A1,A2,A3,A4)
C      RETURN
C      END

C
C      SUBROUTINE ROTZON(IOPT,IZ,A1,A2,A3,A4)
C
C      MULTIPLY SERIES BY COMPLEX NUMBERS
C
C      COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
C      *           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C      NTRMS=IENDI(IZ)-IBEGI(IZ)+1
C      DO 30 I=1,NTRMS
C      I1=IBEGI(IZ)+I-1
C      IF(IOPT.EQ.2)GO TO 10
C      EQU(1,I)=EQUTOT(1,I1)*A1+EQUTOT(2,I1)*A2
C 10 IF(IOPT.EQ.1)GO TO 20
C      EQU(2,I)=EQUTOT(1,I1)*A3+EQUTOT(2,I1)*A4
C 20 IF(IOPT.NE.2)EQUTOT(1,I1)=0.
C 30 IF(IOPT.NE.1)EQUTOT(2,I1)=0.
C      I1=1
C      I2=2
C      IF(IOPT.EQ.1)I2=1
C      IF(IOPT.EQ.2)I1=2
C      CALL PLACE(IZ,I1,I2,I1,I2,1.)
C      RETURN
C      END

C      SUBROUTINE SAVE (IOPT)
C
C      SUBROUTINE TO SAVE EQUATIONS STORED IN ARRAY EQUTOT
C      IF IOPT=0 DON'T DO ANY SCALING
C
C      COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
C      *           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C      IF (IOPT.EQ.0) GO TO 20
C      DO 10 I=1,2
C      DO 10 J=1,NUNK
C 10 IF (ABS(EQUTOT(I,J)).GT.SCALE(J)) SCALE(J)=ABS(EQUTOT(I,J))
C 20 WRITE (IUNIT) ((EQUTOT(I,J),J=1,NN),I=1,2)
C      NWRT=NWRT+1
C      RETURN
C      END

C      SUBROUTINE SCLFIX
C
C      COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
C      *           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C      DO 10 I=1,NUNK
C 10 SCALE(I)=1./SCALE(I)
C      RETURN
C      END

```

```

SUBROUTINE SERINF(IZ,ISERTP,ISTP,INEG,IPOS,IZERO,ICOEF,
*                   IPL,X0,Y0,E,XNU)
C
C          SUBROUTINE TO SET VARIABLES CONTAINING SERIES
C          INFORMATION
C
C          ISERTP      - 1 FOR PHI FUNCTION
C                      2 FOR PSI FUNCTION
C          ISTP        - EXPANSION TYPE
C          INEG        - NUMBER OF NEGATIVE POWERS
C          IPOS        - NUMBER OF POSITIVE POWERS
C          IZERO       - 0 IF ZERO POWER EXCLUDED
C          IOR         - 0 TO EXCLUDE REAL COEF, ODD POWER
C          IOI         - 0 TO EXCLUDE IMAG COEF, ODD POWER
C          IER         - 0 TO EXCLUDE REAL COEF, EVEN POWER
C          IEI         - 0 TO EXCLUDE IMAG COEF, EVEN POWER
C          IPL         - 1 FOR PLANE STRESS
C                      2 FOR PLANE STRAIN
C          (X0,Y0)    - EXPANSION POINT
C          E,XNU      - ELASTIC CONSTANTS
C
C          COMMON /EQN/  EQU(3,100),IBEGI(:0),IENDI(10),EQUTOT(2,175),
*                         SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
C          COMMON /MAT/  G(5),ETAM(5)
C          COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                         NPOS(10),IZRO(10),IODRL(10),
*                         IODIM(10),IEVRL(10),IEVIM(10)
C          DIMENSION ICOF(4)
C          EQUIVALENCE (ICOF(4),IOR),(ICOF(3),IOI),(ICOF(2),IER),
*                         (ICOF(1),IEI)
C          IZ1=IZ
C          IF (ISERTP.EQ.2) IZ1=IZ+5
C          IZONES=MAX0(IZ,IZONES)
C          ISTYP(IZ1)=ISTP
C          NNEG(IZ1)=INEG
C          NPOS(IZ1)=IPOS
C          IZRO(IZ1)=IZERO
C          CALL DECODE(ICOEF,4,ICOF,NDUM)
C          IODRL(IZ1)=IOR
C          IODIM(IZ1)=IOI
C          IEVRL(IZ1)=IER
C          IEVIM(IZ1)=IEI
C          XNOT(IZ1)=X0
C          YNOT(IZ1)=Y0
C          NEVP=INEG/2+IPOS/2
C          NODP=NEVP
C          IF (INEG/2.NE.(INEG+1)/2) NODP=NODP+1
C          IF (IPOS/2.NE.(IPOS+1)/2) NODP=NODP+1
C          IF (IZERO.NE.0) NEVP=NEVP+1
C          NZUNK=NEVP*(IER+IEI)+NODP*(IOR+IOI)
C          IBEGI(IZ1)=NUNKS+1
C          NUNKS=NUNKS+NZUNK
C          IENDI(IZ1)=NUNKS
C          NUNK=NUNKS
C          NN=NUNK+1
C          G(IZ)=E/(2.*(1.+XNU))
C          GO TO (10,20), IPL
10      ETAM(IZ)=(3.-XNU)/(1.+XNU)
20      GO TO 30
30      ETAM(IZ)=3.-4.*XNU
30      RETURN
      END

```

SUBROUTINE SERFIL (IZ,F1,F2,A,B)

C  
C  
C  
C

SUBROUTINE TO FILL EQUATIONS FOR UNKNOWN COEFFICIENTS

```
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                 NPOS(10),IZRO(10),IODRL(10),
*                 IODIM(10),IEVRL(10),IEVIM(10)
IZR=IZRO(IZ)
NT1=NNEG(IZ)+NPOS(IZ)+1
IOR=IODRL(IZ)
IOI=IODIM(IZ)
IER=IEVRL(IZ)
IEI=IEVIM(IZ)
IPOW=-NNEG(IZ)
IEO=1
IP1=ABS(IPOW)
IF (IP1/2.EQ.0.AND.IPOW.EQ.0) IEO=2
IND=1
DO 30 I=1,NT1
IF (IZR.EQ.0.AND.IPOW.EQ.0) GO TO 20
CS=COS(TH(I))
SN=SIN(TH(I))
IF ((IOR.EQ.0.AND.IEO.EQ.1).OR.(IER.EQ.0.AND.IEO.EQ.2)) GO TO 10
EQU(1,IND)=EQU(1,IND)+R(I)*(A*CS-B*F1*SN)
EQU(2,IND)=EQU(2,IND)+R(I)*(B*CS+A*F1*SN)
IND=IND+1
10 IF ((IOI.EQ.0.AND.IEO.EQ.1).OR.(IEI.EQ.0.AND.IEO.EQ.2)) GO TO 20
EQU(1,IND)=EQU(1,IND)-F2*R(I)*(B*CS+A*F1*SN)
EQU(2,IND)=EQU(2,IND)+F2*R(I)*(A*CS-B*F1*SN)
IND=IND+1
20 IPOW=IPOW+1
IEO=3-IEO
30 CONTINUE
RETURN
END
```

SUBROUTINE SLVINT

C  
C  
C  
C

SUBROUTINE TO INITIALIZE VARIABLES FOR SOLUTION ROUTINE

```
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
IDIAG(1)=1
N=NUNK
DO 10 I=1,NUNK
IDIAG(I+1)=IDIAG(I)+N
10 N=N-1
N=IDIAG(NUNK)
DO 20 I=1,N
20 A(I)=0.
DO 30 I=1,NUNK
30 PHI(I)=0.
RETURN
END
```

```

SUBROUTINE STCOL(XP,YP,N,IZ,IREF,ALPHA,RHS1,RHS2,IERR)

SUBROUTINE TO COMPUTE STRESS EQUATIONS
MEANING OF IREF

1 - NO REFLECTIONS
2 - X-AXIS REFLECTION
3 - UNIT CIRCLE REFLECTION
ALPHA - ANGLE OF NORMAL TO SURFACE ON WHICH TO FIND STRESS

DIMENSION XP(1),YP(1),RHS1(1),RHS2(1),ALPHA(1)
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /PIFAC/ PI,HLFPI,TWOP1
DO 20 I=1,N
CALL ZERO(0.0,0.1,2.1,0)
ALFA=PI*ALPHA(I)/180.
CALL STRT(XP(I),YP(I),IZ,ALFA,IREF,1.,1,2,1,2)
EQUTOT(1,NN)=RHS1(I)
EQUTOT(2,NN)=RHS2(I)
IF(IERR.EQ.1)GO TO 10
CALL SAVE(1)
GO TO 20
CALL EVAL(1,2,2,XER,YER)
PRINT 30, XER,YER,XP(I),YP(I)
CONTINUE
RETURN
FORMAT(1H ,2F10.4,2E10.4)
END

```

## SUBROUTINE SOLVE

## SUBROUTINE TO SOLVE SIMULTANEOUS EQUATIONS

```

COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /SOLN/ A(15401),IDIAG(176),PHI(176)
EQUIVALENCE (N,NUNK)
DIMENSION T(176)
DO 70 I=1,N
L=IDIAG(I)
TEMP=A(L)
LL=IDIAG(I+1)-1
II=I-L
DO 10 J=L,LL
T(II+J)=A(J)
10 A(J)=A(J)/TEMP
PHI(I)=PHI(I)/TEMP
DO 60 J=1,N
MM=IDIAG(J+1)-1
NOFF=LL-MM
IF (J-I) 20,60,30
20 M=IDIAG(J)+I-J
TEMP=A(M)
GO TO 40
30 M=IDIAG(J)
TEMP=T(J)
40 DO 50 K=M,MM
50 A(K)=A(K)-TEMP*A(K+NOFF)
PHI(J)=PHI(J)-TEMP*PHI(I)
60 CONTINUE
70 CONTINUE
RETURN
END

```

```

SUBROUTINE STITCH (NZ1,NZ2,NREF1,NREF2,ISOPT,INV,
1           INVZN,NPT,XX,YY,F1,F2,U,V,IERR)

C
C
C      SUBROUTINE TO STITCH TWO ZONES
C      ISOPT      - 1--STITCH FORCES ONLY
C                  2--STITCH DISPLACEMENTS ONLY
C                  3--STITCH FORCES,DISPLACEMENTS
C      INV       - 1--POINTS COMING FROM PARAMETER PLANE
C                  OF ZONE INVZN
C      IERR      - 0 IF NOT CALCULATING ERRORS

C
C
C      COMMON /EQN/  EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*                  SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
COMMON /MAT/  G(5),ETAM(5)
DIMENSION XX(1), YY(1), F1(1), F2(1), U(1), V(1)
IREF1=NREF1
IREF2=NREF2
IZ1=NZ1
IZ2=NZ2
IF (INV.EQ.2.0R.INVZN.EQ.NZ1.AND.INV.EQ.1) GO TO 10
IREF1=NREF2
IREF2=NREF1
IZ1=NZ2
IZ2=NZ1
10 IFU1=1
IFU2=2
IF (ISOPT.EQ.1) IFU2=1
IF (ISOPT.EQ.2) IFU1=2
DO 90 I=1,NPT
GO TO (20,30), INV
20 XP1=XX(1)
YP1=YY(I)
GO TO 40
30 X=XX(I)
Y=YY(I)
40 CALL MAPPER (XP1,YP1,X,Y,IZ1,INV)
CALL MAPPER (XP2,YP2,X,Y,IZ2,2)
DO 90 J=IFU1,IFU2
FACT=-1.
IF(J.EQ.2)FACT=-G(IZ1)/G(IZ2)
CALL ZERO (0,0,1,2,1,0)
CALL PTCOL (XP1,YP1,IZ1,J,IREF1,1,1,2,1,2)
IF(IREF1.EQ.4)CALL MLTDSP(XP1,YP1,IZ1)
CALL PTCOL (XP2,YP2,IZ2,J,IREF2,FACT,1,2,1,2)
IF(IREF2.EQ.4)CALL MLTDSP(XP2,YP2,IZ2)
GO TO (50,60), J
50 EQUTOT(1,NN)=F1(I)
EQUTOT(2,NN)=F2(I)
GO TO 70
60 EQUTOT(1,NN)=U(I)
EQUTOT(2,NN)=V(I)
70 IF (IERR.EQ.0) GO TO 80
CALL EVAL (1,2,2,XER,YER)
PRINT 100, XER,YER,XP1,YP1,XP2,YP2
GO TO 90
80 CALL SAVE (1)
90 CONTINUE
RETURN
100 FORMAT (1H ,2F10.4,4E10.4)
END

```

```

SUBROUTINE STRPT(XP,YP,IZ,ALFA,IREF,WT,IF1,IF2,IT1,IT2)

```

```

C
C
C      SUBROUTINE TO COLLOCATE STRESSES AT A POINT
C      XP + I YP - POINT AT WHICH TO COLLOCATE

```

```

C      IZ      - ZONE NUMBER
C      ALFA    - ANGLE OF NORMAL TO SURFACE AT WHICH STRESS I
C      IREF    - REFLECTION OPTION
C          1 -- NO REFLECTIONS
C          2 -- X-AXIS REFLECTION
C          3 -- UNIT CIRCLE REFLECTION
C      WT      - WEIGHTING OF EQUATIONS
C

ALPHA=-ALFA
CSA=COS(2.*ALPHA)
SNA=SIN(2.*ALPHA)
CALL ZERO(1,2,0,0,0,0)
IF(IF1.GT.1)GO TO 10
CALL MAPPR(XP,YP,A,B,IZ)
DENOM=1./(A*A+B*B)
AA=2.*A*DENOM
BB=-2.*B*DENOM
CALL PHIPB(XP,YP,AA,-BB,IZ)
CALL ZERO(2,2,0,0,0,0)
10 CALL B4PHDP(XP,YP,IZ,CSA,SNA,IREF,A,B)
CALL PHIPPB(XP,YP,A,-B,IZ)
CALL B4PHP(XP,YP,CSA,SNA,IZ,IREF,A,B)
CALL PHIPB(XP,YP,A,-B,IZ)
CALL MAPPR(XP,YP,XPR,YPR,IZ)
CSA=COS(2.*ALPHA)
SNA=SIN(2.*ALPHA)
DENOM=1./*(XPR+XPR+YPR+YPR)
A=DENOM*(CSA*XPR+SNA*YPR)
B=DENOM*(SNA*XPR-CSA*YPR)
GO TO (40,20,30),IREF
20 CALL PHIBP1(XP,YP,A,-B,IZ)
GO TO 40
30 XT=XP+XP-YP+YP
YT=2.*XP+YP
DENOM=1./*(XT+XT+YT+YT)
AA=-DENOM*(A*XT+B*YT)
BB= DENOM*(A*YT-B*XT)
CALL PHIPB(XP,YP,AA,-BB,IZ)
40 CALL PLACE(IZ,IF1,IF2,IT1,IT2,WT)
IF(IREF.NE.1)GO TO 50
A=-A
B=-B
CALL ZERO(1,2,0,0,0,0)
CALL PHIPB(XP,YP,A,-B,IZ+5)
CALL PLACE(IZ+5,IF1,IF2,IT1,IT2,WT)
50 RETURN
END

```

SUBROUTINE STRRES (IZ,NPT,IREF,ALFA,X,Y,XP,YP)

```

C
C      SUBROUTINE TO COMPUTE AND PRINT STRESSES FROM SOLUTION
C
C      IREF      - 1 FOR NO REFLECTIONS
C                  2 FOR X-AXIS REFLECTION
C                  3 FOR UNIT CIRCLE REFLECTION
C      ALFA      - ANGLES OF NORMAL TO SURFACES ON WHICH ST
C                  ARE CALCULATED
C
```

```

DIMENSION X(1), Y(1), XP(1), YP(1), ALFA(1)
COMMON /PIFAC/ PI,HLFPI,TWOP
FACT=180./PI
PRINT 20
DO 10 I=1,NPT
CALL ZERO (0,0,1,2,3,0)
CALL STRPT (XP(I),YP(I),IZ,ALFA(I),IREF,1.,1,2,1,2)

```

```

CALL EVAL (1,2,1,SIG,TAU)
CALL ZERO(0,0,1,2,3,0)
CALL STRPT(XP(I),YP(I),IZ,ALFA(I)+HLFPI,IREF,1.,1,1,1,1)
CALL EVAL(1,1,1,SIG90,SDUM)
ALF=ALFA(I)*FACT
10 PRINT 30, SIG,SIG90,TAU,ALF,X(I),Y(I),XP(I),YP(I)
RETURN
20 FORMAT (////23H0EVALUATION OF STRESSES / 7X,7HSTRESS1,
*           6X,7HSTRESS2,1X,12HSHEAR STRESS,5X,5HANGLE,
*           9X,1HX,12X,1HY,8X,8HX(PARAM),5X,8HY(PARAM) )
30 FORMAT (1X,3E13.5,F10.3,4E13.5)
END

```

```

FUNCTION TANGO (X1,X2)
TANGO=BRANCH(ATAN2(X1,X2),0.)
RETURN
END

```

```

C SUBROUTINE UNIT(I)
C SUBROUTINE TO SET UP NEW TAPE FOR WRITING EQUATIONS
C
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*           SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
IUNIT=I
NWRT=0
RETURN
END

C SUBROUTINE WRTDSP(NFB,NFD,IZ,IREF)
C ROUTINE TO WRITE DISPLACEMENTS AT INTERFACE
C OF MMC AND FINITE ELEMENT REPRESENTATIONS FOR
C BACKSUBSTITUTION INTO FINITE ELEMENT EQUATIONS
C
COMMON /MAT/ G(5),ETAM(5)
COMMON /MMCCE/ X(150),Y(150),FDRHS(300),EQNS(120,176),
*           KUV(120,2)
* DIMENSION FD(1)
EQUIVALENCE (FD(1),FDRHS(1))
REWIND NFB
REWIND NFD
READ (NFB) N1,N2,IDOFS
NPT=N2/2
READ (NFB) (X(I),Y(I),I=1,NPT)
A=1.
B=0.
DO 100 I=1,NPT
CALL ZERO(0,0,1,2,1,0)
CALL MAPPER(XP,YP,X(I),Y(I),IZ,2)
CALL PTCOL(XP,YP,IZ,2,IREF,1.,1,2,1,2)
IF(IREF.EQ.4)CALL MAPPR(XP,YP,A,B,IZ)
FACT=1./((A*A+B*B)*2.*G(IZ))
CALL EVAL(1,2,1,V1,V2)
FD(2*I-1)=(V1*A-V2*B)*FACT
100 FD(I-2)=(V1*B+V2*A)*FACT
WRITE (NFD) (FD(I),I=1,N2)
END FILE NFD
RETURN
END

```

```

C SUBROUTINE ZETN(XP,YP,IZ)
C
C     ROUTINE TO CALCULATE TERMS
C     IN EXPANSION OF PHI, PSI
C
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                  NPOS(10),IZRO(10),IODRL(10),
*                  IODIM(10),IEVRL(10),IEVIM(10)
ITYP=ISTYP(IZ)
GO TO (10,20),ITYP
10 A=1.
B=0.
GO TO 40
20 YY=YP+1.
DEN=1. / (XP*XP+YY*YY)
A= XP-DEN
B=-YY-DEN
40 CALL POWSER(XP,YP,A,B,IZ)
RETURN
END

```

```

C SUBROUTINE ZERO (IE1,IE2,IS1,IS2,IOPT,IINPT)
C
C     SUBROUTINE TO ZERO OUT ZONE AND MASTER EQUATIONS
C
IE1,IE2      -BEGINNING AND ENDING EQUATION TO ZERO OUT
              (ZONE EQUATIONS)
IS1,IS2      -BEGINNING AND ENDING EQUATION TO ZERO OUT
              (MASTER EQUATIONS)
IOPT         -OPTION FOR ZEROING OUT MASTER EQUATIONS
              1--ZERO UP TO CONSTANTS
              2--ZERO TO TOTAL UNKNOWNS
              3--ZERO TO TOTAL UNKNOWNS +1 (RHS)
              4--ZERO TO UNKNOWN IINPT
C
COMMON /EQN/ EQU(3,100),IBEGI(10),IENDI(10),EQUTOT(2,175),
*                  SCALE(175),NN,NUNKS,NUNK,NWRT,IUNIT
IF (IE2-IE1.LT.0.OR.(IE2.EQ.0.AND.IE1.EQ.0)) GO TO 20
DO 10 I=IE1,IE2
DO 10 J=1,100
10 EQU(I,J)=0.
20 IF (IS2-IS1.LT.0.OR.(IS2.EQ.0.AND.IS1.EQ.0)) RETURN
NT=NUNKS
IF (IOPT.EQ.2) NT=NUNK
IF (IOPT.EQ.3) NT=NN
IF (IOPT.EQ.4) NT=IINPT
DO 30 I=IS1,IS2
DO 30 J=1,NT
30 EQUTOT(I,J)=0.
RETURN
END

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C SUBROUTINE ZETN1(XP,YP,IZ)
C
C     ROUTINE TO COMPUTE TERMS IN FIRST
C     DERIVATIVE OF EXPANSION FOR PHI, PSI
C
DIMENSION RT(100),TT(100)
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                  NPOS(10),IZRO(10),IODRL(10),
*                  IODIM(10),IEVRL(10),IEVIM(10)
NTOT1=NNEG(IZ)+NPOS(IZ)+1
ITYP=ISTYP(IZ)

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      GO TO (10,20),ITYP
10  A=1.
    B=0.
    GO TO 40
20  YP1=YP+1.
    DAB=1. / (XP*XP+YP1*YP1)
    DCD=DAB*DAB
    A= XP*DAB
    B=-YP1*DAB
    C=DCD*(YP1-YP1-XP*XP)
    D=DCD*XP*YP1*2.
40  CALL PWSERD(XP,YP,A,B,IZ)
    IF(ITYP.EQ.1)GO TO 60
    DO 50 I=1,NTOT1
    RT(I)=R(I)
50  TT(I)=TH(I)
    CALL POWSER(XP,YP,C,D,IZ)
    CALL RADD(RT,TT,NTOT1)
60  RETURN
END

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SUBROUTINE ZETN2(XP,YP,IZ)
C
C      ROUTINE TO COMPUTE TERMS IN SECOND
C      DERIVATIVE OF EXPANSION FOR PHI, PSI
C
DIMENSION RT(100),TT(100)
COMMON /PIFAC/ PI,HLFPI,TWOP
COMMON /POWERS/ R(100),TH(100),ISHFT
COMMON /SERIES/ ISTYP(10),IZONES,XNOT(10),YNOT(10),NNEG(10),
*                  NPOS(10),IZRO(10),IODRL(10),
*                  IODIM(10),IEVRL(10),IEVIM(10)
NTOT1=NNEG(IZ)+NPOS(IZ)+1
ITYP=ISTYP(IZ)
GO TO (10,20),ITYP
10  A=1.
    B=0.
    GO TO 30
20  YP1=YP+1.
    DEN=1. / (XP*XP+YP1*YP1)
    A= XP*DEN
    B=-YP1*DEN
30  CALL PWSRD2(XP,YP,A,B,IZ)
    IF(ITYP.EQ.1)GO TO 60
    DO 40 I=1,NTOT1
    RT(I)=R(I)
40  TT(I)=TH(I)
    CALL ZETN1(XP,YP,IZ)
    DEN=2.*SQRT(DEN)
    TTH=-ATAN2(YP1,XP)+PI
    DO 50 I=1,NTOT1
    R(I)=R(I)*DEN
50  TH(I)=BRANCH(TH(I)+TTH,-PI)
    CALL RADD(RT,TT,NTOT1)
60  RETURN
END

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